# LEVEL BOOK

14.113.0028

O.K.

No. 43261
MADE BY
The Hicks-Judd Company
Bookbinders, Printers
Loose Leaf Systems
51-65 First St. San Francisco
** Give above number when ordering Duplicate

7°26'

3°38

Lock Padden & Co.
35 Montgomery St.
SF.
Sub. Div. = #2

{Pedrena & De Vato.
Willo Creek} Lumber

Level Book 1.

# INDEX.


Notes on Markham Br. - 1-10
" " Cazadero - 11-21
" " Markham Br 23-26
" " " " 29-34
" " County Road Markham Br 35-37
" Laton Lumber Spur 38-59
" Spur for P.P.+K. 60-61
Re alignment of Laton Spur 62-63
Line Change Mark. Br near Rocky Pt. 65
Temporary Trestle & Washout - 28

E 1347

M 0+84.7

E 1346 Road, 17+55

M 0+00

E 1345+59.45 =

E 1345+50

E 1345 Road 16+80

E 1344+50 Road 16+00

E 1344

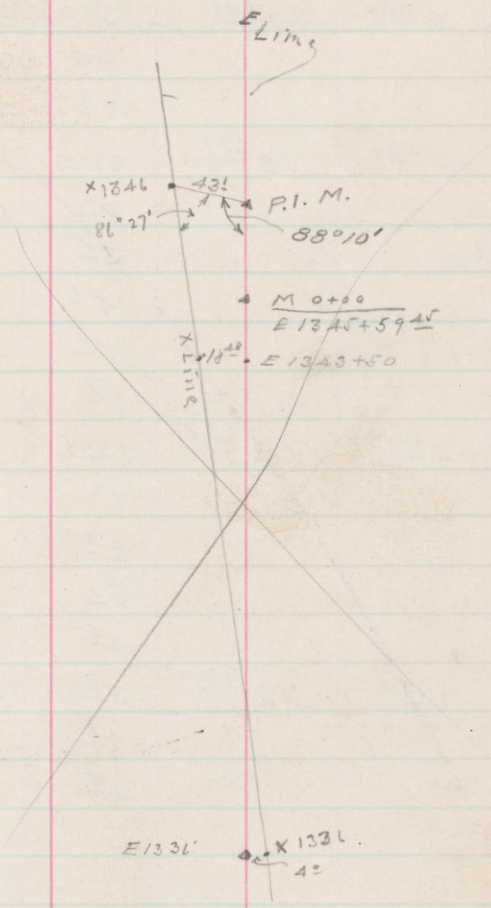
E 1343+50 Road 15+10

# Markham Branch.

| | | | | | | |
|---|---|---|---|---|---|---|
| 00/00 | +12 5/8 / 15 | +24 5/8 / 25 | +36 / 36 | +48 / 51 | +60 / 62 | +72 / 83 | +73 5/8 / 90 |
| 00/00 | | | | | +67 / 76 | | |
| 00/00 | +18 1/2 / 17 | +30 1/2 / 29 | +42 / 42 | +54 / 53 | +66 / 69 | +70 / 77 | |
| 00/00 | +12 / 16 | +24 / 33 | +34 / 48 | -38 1/2 / 56 5/8 | +50 1/2 / 69 | +59 3/8 / 86 | |
| 00/00 | +12 / 17 | +24 4/8 / 35 1/2 | +36 4/8 / 50 | +48 1/2 / 70 | +59 / 87 | +56 / 94 | |
| 00/00 | +12 / 18 | +23 5/8 / 38 | +35 2/8 / 67 | +47 2/8 / 100 | +60 / 125 4/8 | | |
| 00/00 | +11 2/8 / 19 2/8 | +23 4/8 / 38 1/8 | +35 4/8 / 72 4/8 | +47 4/8 / 105 5/8 | +56 3/8 / 119 4/8 | | |
| 00/00 | +7 2/8 / 14 8/8 | +9 4/8 / 18 5/8 | +21 2/8 / 37 2/8 | +33 1/8 / 76 8/8 | +44 3/8 / 101 4/8 | | |

| | | | |
|---|---|---|---|
| X1346 △ | | 35 f Lt Bank | 13° Rt fence |
| 1345 | | 20 ft. Lt Bank | 12° Rt fence |
| 1344 | | 7 ft Lt to Top Bank | 9° Rt |
| +47 | △ | | |
| +25. | | Top of Bank. | |
| 1343 | | 4 ft Lt = fence | |
| 1342 | | 11 ft Lt = fence | |
| 1341 | | 3 ft Lt = fence | |
| 1340 | | 2 ft Rt = fence | |
| 1339 | | 4 ft. Rt = fence | |
| +80 | | fence | |
| 1338 | | | |
| 1337 | | 10 ft Lt. to fence | |
| X1336 | △ | | |
| E1336 - 4 ft Rt = | | | |

900
240
670


E Line
X1346
43'
P.I. M.
86°27'
88°10'
M 0+00
E 1345+59 45
X Line
18 48
E 1343+50
E1336
X 1336
4°

| | | | | |
|---|---|---|---|---|
| B.M | 2.000 | 20.641 | | 18.641 |
| X1346 | | | 9.4 | 11.2 |
| 1345 | | | 9.6 | 11.0 |
| T.P | 1.030 | 19.671 | 2.000 | 18.641 |
| 1344 | | | 8.5 | 11.2 |
| 1343 +47 Δ | | | 3.8 | 15.9 |
| 1343 | | | 5.1 | 14.6 |
| 1342 | | | 5.1 | 14.6 |
| 1341 | | | 7.7 | 12.0 |
| T.P | 4.970 | 18.636 | 6.005 | 13.666 |
| 1340 | | | 8.2 | 10.4 |
| 1339 | | | 8.2 | 10.4 |
| 1338 | | | 5.0 | 13.6 |
| 1337 | | | 4.0 | 14.6 |
| T.P | 7.994 | 22.830 | 3.800 | 14.836 |
| X1336 | | | 2.9 | 19.9 |
| E1336 | | | 4.4 | 18.4 |

B.M. #12 on Bay Tree Elev. 18.61

TP

T.P.

Marcham Branch

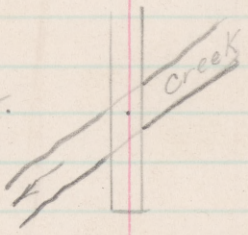
Mar-7-1913

| | | | |
|---|---|---|---|
| E 1344 | | | |
| +50 | P.O.T. | | |
| 1343 | | | |
| 1342 | | | |
| 1341 | | | |
| 1340 | | | |
| 1339+60 | | | |
| 1338+90 | | | |
| +50 | | | |
| 1338+01.5 | E.C. Δ | | |
| 1336+86.5 | C.C.T 2¾ Δ | | 13° 39' ✓ |
| +50 | | | 11° 49.5 ✓ |
| 1336 | | Δ 39°18 | 9° 19.5 ✓ |
| +50 | | St+t. 26.5 16 | 6° 49.5 ✓ |
| 1335 | | | 4° 19.5 ✓ |
| 1334+50 | | | 1° 49.5 ✓ |
| X 1334+13.5 | C.C 10° 47 Δ | | 0° 00 ✓ |
| X 1332+93.5 | B.C.T-2¾ Δ | | |
| X 1332+60.20 | P.O.T. Δ | | |
| E 1332+60.20 | B.C. | | |
| E 1331+76.9 Δ | E.C. | | |

Markham Branch

Mar. 7-1912

+60 Cent Creek.




+40° Beg Trash

1351

1350+85 4 △ C.C. 14° ℄ of Pres Track

+50 2°29' ✓

1350 5°59' ✓

+50 9°29' ✓ △ 62°14

1349 12°59 ✓ St. 317 83 P.I. to C.C.

+50 △ 16°29 ✓ Stt. 401 85 P.I. to B.C.

1348 19°59 ✓ Total △ 74°50'

+50 △ 7°38' ✓

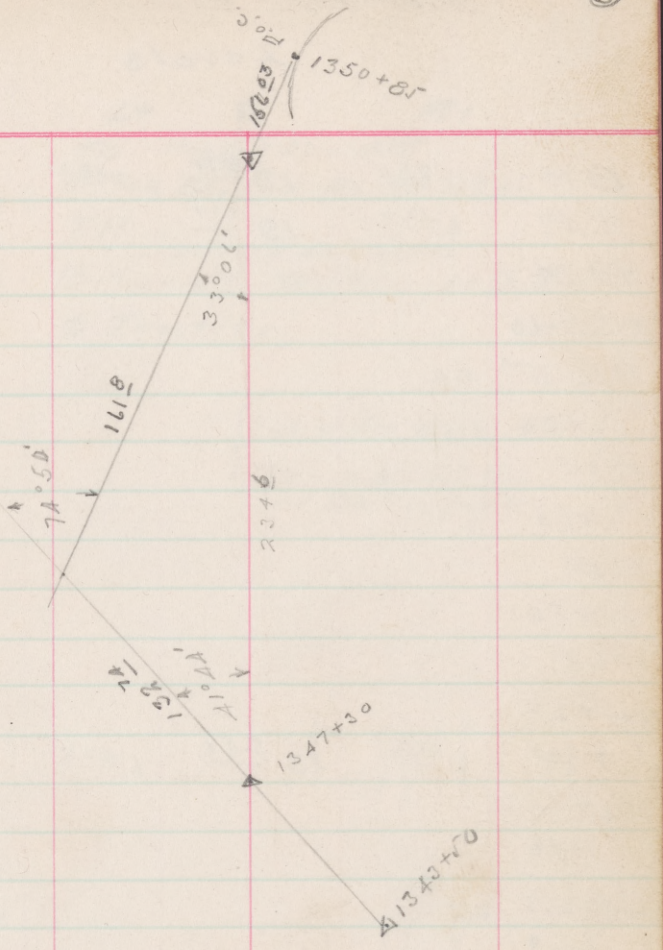
1347 4°08' ✓

+50 0°38' ✓

1346+40 9 △ C.C. 14° Pt.

△ 12°36'

×1344+60 9 △ B.C. 2 3/4


1350+85
1618
3300'
74°50'
R346
1347+30
1343+70

# Markham Br.

## Levels.

| | + | * | − | F.S. |
|---|---|---|---|---|
| B.M. | 1 230 | 19 871 | 7 180 | |
| T.P. | 6 420 | 19 111 | | |
| B.M. | | | | 4 855 |
| X1351+60 | | | | 5 3 |
| 1350+85 | c.c | | | 5 7 |
| +50 | | | | 5 8 |
| 1350 | | | | 5 8 |
| +50 | | | | 5 6 |
| 1349 | | | | 5 2 |
| +50 | | | | 7 1 |
| 1348 | | | | 8 6 |
| 1347+50 | | | | 9 4 |
| T.P. | 0 860 | 13 551 | 6 420 | |
| 1347 | | | | 3 8 |
| +50 | | | | 4 8 |
| 1346+40 | c.c. | | | 4 7 |
| +10 | | | | 1 3 |
| 1345+80 | | | | 3 8 |
| +50 | | | | 2 4 |
| T.P. | 9 200 | 20 451 | 2 300 | |
| 1345+20 | | | | 8 8 |
| 1344+90 | | | | 9 4 |
| +60 | B.C. | | | 9 6 |
| +50 | | | | 9 5 |
| 1344 | | | | 8 6 |
| +50 | | | | 5 0 |
| 1343 | | | | 5 8 |

| | Lt ℄ Rt. |
|---|---|
| 18 $\frac{641}{}$ | #12 Marked Elev 18 $\frac{641}{}$ |
| | 8 Mon Bay Tree Rt. Sta 1345. |
| 12 $\frac{691}{}$ | T.P. |
| 14 $\frac{256}{}$ | Marked Elev 14.256 |
| | B.M. on old R.W. Tree. Lt Sta. 1350+25 |
| 13 $\frac{8}{}$ | ℄ Trestle |
| 13 $\frac{4}{}$ | |
| 13 $\frac{1}{}$ | { High Water Elev 19 $\frac{155}{}$ |
| 13 $\frac{3}{}$ | Blaze on R.W. Tree. |
| 13 $\frac{5}{}$ | at Sta 1350+25 } |
| 13 $\frac{9}{}$ | |
| 12 $\frac{0}{}$ | |
| 10 $\frac{5}{}$ | |
| 9 $\frac{7}{}$ | |
| 12 $\frac{691}{}$ | |
| 9 $\frac{8}{}$ | |
| 8 $\frac{8}{}$ | |
| 9 $\frac{3}{}$ | |
| 12 $\frac{3}{}$ | |
| 9 $\frac{8}{}$ | |
| 11 $\frac{2}{}$ | |
| 11 $\frac{25'}{}$ | T.P. |
| 11 $\frac{7}{}$ | |
| 11 $\frac{1}{}$ | |
| 10 $\frac{9}{}$ | |
| 11 $\frac{0}{}$ | |
| 11 $\frac{9}{}$ | |
| 15 $\frac{5}{}$ | Grade 19 $\frac{0}{}$ $-\frac{35}{00}$ $+\frac{90}{30}$ $+\frac{21}{47}$ $+\frac{288}{59}$ |
| 14 $\frac{7}{}$ | |

Markham Branch.

| | | | | |
|---|---|---|---|---|
| 1342+50 | | 20 45 1 | | 1 1 |
| 1342 | | | | 5 8 |
| +50 | | | | 6 2 |
| 1341 | | | | 7 2 |
| +50 | | | | 7 1 |
| T.P. | 5 4 2 0 | 18 5 6 1 | 7 3 1 0 | |
| 1340 | | | | 6 0 |
| 1339+60 | | | | 6 0 |
| 1338+90 | | | | 5 2 |
| +50 | | | | 6 6 |
| T.P. | 10 6 1 0 | 23 7 9 6 | 5 3 7 5 | |
| 1338+06 5 | E.C. | | | 2 9 |
| +76 5 | | | | 8 5 |
| +46 5 | | | | 8 3 |
| 1337+16 5 | | | | 7 1 |
| +86 5 | C.C. | | | 4 2 |
| +50 | | | | 3 0 |
| 1336 | | | | 6 2 |
| +85 | | | | 6 6 |
| +60 | | | | |
| +50 | | | | 2 6 |
| 1335+35 | | | | 6 2 |
| +15 | | | | 0 4 |
| 1335 | | | | 4 4 |
| +70 | | | | 6 1 |
| +50 | | | | 2 4 |
| 1334+13 5 | C.C. | | | 8 9 |

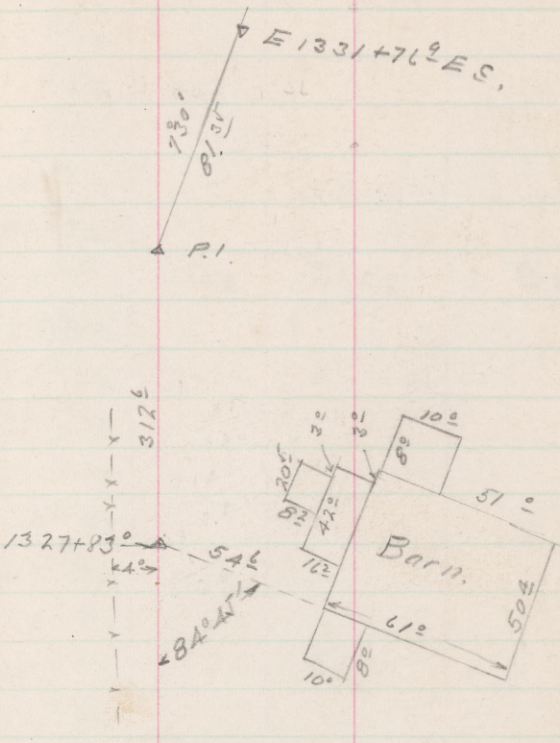
| | Lt | ℄ | Rt. | | |
|---|---|---|---|---|---|
| $14^{4}$ | | | | | |
| $14^{7}$ | Grade $19^{0}$ | $-4^{3}$ / 00 | $+29^{6}$ / 60 | | |
| $14^{3}$ | | $-4^{7}$ / 00 | | | |
| $13^{3}$ | | $-5^{7}$ | | | |
| $12^{8}$ | | $-6^{2}$ / 00 | | | |
| $13^{141}$ | T.P. | | | | |
| $12^{6}$ | | $-6^{4}$ / 00 | | | |
| $12^{6}$ | | $-6^{4}$ / 00 | | | |
| $13^{4}$ | Grade $19^{0}$ | $-5^{6}$ / 00 | $+6^{6}$ / 60 | | |
| $12^{0}$ | | $+7^{0}$ / 00 | | | |
| $13^{186}$ | T.P. | | | | |
| $20^{9}$ | $-5^{6}$ / $9^{0}$ | $+1^{9}$ / 00 | $+7^{5}$ / 15 | | |
| $15^{3}$ | | $-3^{7}$ / 00 | | | |
| $15^{5}$ | | $-3^{5}$ / 00 | | | |
| $16^{7}$ | | $-2^{3}$ / 00 | | | |
| $19^{6}$ | $-4^{6}$ / $10^{0}$ $-4^{6}$ / $4^{0}$ | $+0^{6}$ / 00 | $+13^{4}$ / 20 | $+16^{8}$ / 30 | $+22^{8}$ / 50 |
| $20^{8}$ | | $+1^{8}$ | | | |
| $17^{6}$ | $-2^{8}$ / 17 $-2^{8}$ / $2^{0}$ | $-1^{4}$ / 00 | $+13^{0}$ / 50 | | |
| $17^{2}$ | | $-1^{8}$ | | | |
| $26^{3}$ | | $+7^{3}$ | | | |
| $21^{2}$ | $-3^{4}$ / 18 $-3^{4}$ / $6^{5}$ | $+2^{2}$ / 00 | $+9^{6}$ / 15 | $+12^{8}$ / 30 | $+16^{6}$ / 60 |
| $17^{6}$ | | | | | |
| $23^{4}$ | | | | | |
| $19^{4}$ | | | | | |
| $17^{7}$ | | | | | |
| $21^{4}$ | $-3^{2}$ / 22 $-3^{2}$ / $9^{0}$ | $+2^{4}$ / 00 | $+13^{4}$ / 60 | | |
| $14^{9}$ | | | | | |

| | | | | |
|---|---|---|---|---|
| 1333+83 5 | | 23 796 | | 10 3 |
| +53 5 | | | | 11 2 |
| 1333+23 5 | | | | 11 2 |
| 1332+93 5 B.C. | | | | 6 6 |
| T.P. Δ 1 84 | | 25 166 | 3 470 | |
| 1332+60 3 P.O.T. | | | | 3 5 |
| +50 | | | | 4 0 |
| +17 34 E.C. | | | | 4 1 |
| 1332 | | | | 6 0 |
| +50 | | | | 3 9 |
| 1331 | | | | 2 8 |
| +50 | | | | 6 0 |
| 1330 | | | | 8 2 |
| +63 45 B.C. | | | | 8 1 |
| +50 | | | | 8 1 |
| 1329 | | | | 9 1 |
| +50 | | | | 8 4 |
| 1328+42 77 E.C. | | | | 8 5 |
| T.P. | 8 354 | 25 310 | 8 210 | |
| 1328+12 77 | | | | 8 2 |
| 1327+82 77 C.C. | | | | 7 2 |
| +50 | | | | 6 5 |
| +10 | | | | 5 0 |
| +05 | Pitch. | | | 8 9 |
| +02 | | | | 7 9 |
| 1327 | | | | 5 0 |
| +50 77 C.C. | | | | 7 0 |

| | |
|---|---|
| 13 5/5 | -5 5/5 |
| 12 6/6 | -6 4/6 |
| 12 6/6 | -6 4/6 |
| 17 2/2 | -1 2/2 |
| 20 3/3 2/2 6/6 | T.P. on A |
| 20 3/3 | +1 3/3 |
| 21 2/2 | +2 2/2 |
| 21 1/1 | +2 1/1 |
| 19 2/2 | +0 2/2 |
| 21 3/3 | +2 3/3 |
| 22 4/4 | +3 4/4 |
| 19 2/2 | +0 2/2 |
| | 0/0 |
| 17 0/0 | -2 0/0 |
| 17 1/1 | -1 1/1 |
| | 0/0 |
| 17 1/1 | -1 1/1 |
| | 0/0 |
| 16 1/1 | -2 1/1 |
| 16 8/8 | -2 2/8 |
| 16 7/7 | -2 3/7 |
| 16 9/9 5/5 6/6 | |
| 17 1/1 | -1 1/9 |
| 18 1/1 | -0 1/9 |
| 18 8/8 | -0 2/8 |
| 20 3/3 | +1 3/3 |
| 18 4/4 | -2 1/6 |
| 17 4/4 | -1 1/6 |
| 20 3/3 | +1 3/3 |
| 18 3/3 | -0 1/7 |

Cont - Page (10)

| | | | | |
|---|---|---|---|---|
| X 1332+60² / E 1332+60² | P.O.T. | | | |
| E 1331+76⁰ | E.C. | | | |
| +81 35 | | | | |
| 1330+95.55 | P.I. | 7°30 Rt. | | |
| 3 12 ⁰ | | | | |
| 1327+83⁰ | △ | | | |
| | | | 9' | |
| 1323+92 87 | E.C. | | | |
| +17 87 | C.C. 10°27! | | | |
| E 1323. | 9° 06½ | | +03.54 / 9.4 / +12.94 | |
| +50 | 5° 21½ | | | |
| E 1322+00 | 1° 36½ | | | |
| E 1321+78 54 | C.C. | | | |
| 1321+03 54 | B.C. | on Trestle | | |


E 1331+76.9 E.S.
73°30'
81.35
P.I.
312.6
1327+83°
4°
54.6
84°45'
3°
3°
10°
8°
20.5
8.2
42°
16.2
51°
Barn.
61°
50.4
10°
8°

Markham Branch

Cont'd fr. P. 8

| | | | | |
|---|---|---|---|---|
| 1326+21 77 | | 25 21 | | 7 7 |
| +91 77 B.C. | | | | 8 9 |
| 1325+50 | | | | 8 7 |
| 1325 | | | | 7 1 |
| +50 | | | | 5 7 |
| 1324+05 13 E.C. | | | | 4 4 |
| TP | 4 45 | 27 10 | 2 66 | |
| 1323+60 13 | | | | 5 90 |
| 1323+30 13 C.C. | | | | 4 7 |
| 1323 | | | | 5 1 |
| +50 | | | | 7 1 |
| 1322 | | | | 6 5 |
| 1321+90 8 C.C. | | | | 6 4 |
| +60 8 | | | | 6 4 |
| +30 8 | | | | 5 9 |
| 1321+15 8 D.C. | | | | 5 8 |
| B.M. | | | 7 734 | |

1324+43 2 by "Riordan."
1321+15 8 B.C.

Diff. 27 2

17 6
16 4
16 6
18 2
19 6
20 9
22 65
21 2
22 4
22 0
20 0
20 6
20 7 Base of Rail
20 7
21 2
21 3
19 366 B.M. Spike in Last Bent of Trestle at St 1321+45
Elev. 25.104 ✓ by R. (B. RL B 3 BL)

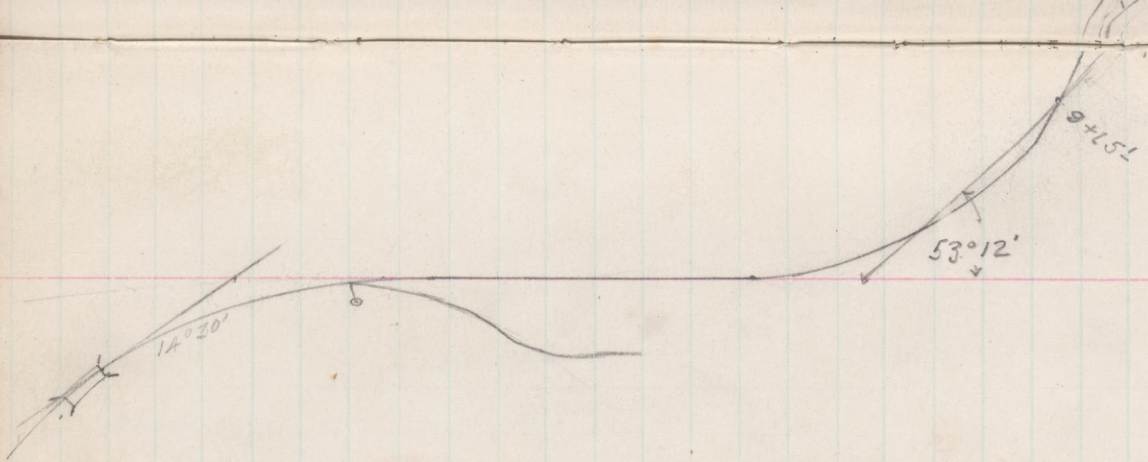
dl 5.738 ✓

# Cazadero

Mar 25-1913

| | |
|---|---|
| +81 3 | Pt Frog. |
| +64 4 | Pt Frog. Crock. |
| 10 +43 0 | Pt Sw 3-4 |
| +97 5 | Pt Frog. |
| +65 1 | Δ 10°50' Lt. |
| +63 7 | Pt Sw. 2 |
| 9 | |
| 8 | |
| +41 1 | ℄ Track |
| 7 | |
| +82 5 | Δ 53°12' Lt. |
| 6 | |
| +31 9 Δ | Apx. B.C. |
| 5 | |
| 4 | |
| 3 | |
| 2 | |
| +31 2 | Pt Sw. #1 Rt. 9 4 |
| 1+03 1 Δ | Pt. 18°50 |
| 1 | |
| 0+00 | East End Trestle 83-E. |

10°50' Lt


9+15±
53°12'
14°30'

Cazadero

Mar 25-1913

26+17.8 △

23

22+89.2 fence

22+48.7 △ 35°13' Rt.

22+29.0 fence.

21+95 fence

20+03.2 △

19

18

+21.1 △ 13°10' Lt

17

16

15

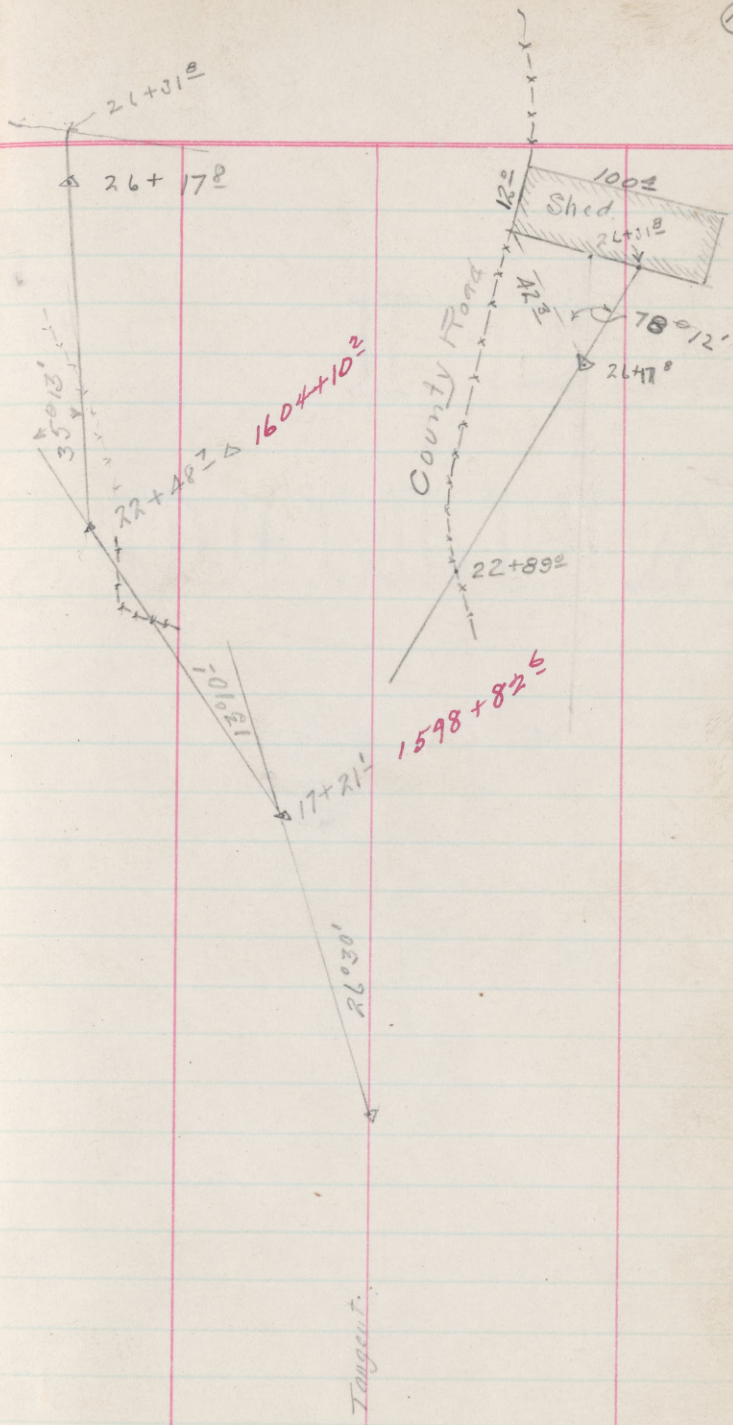
+78.6 △ 26°30' Lt.

14

13

12

11


26+31.8
26+17.8
35°13'
22+48.7
1604+10.2
12°10'
17+21.1
1598+82.6
26°30'
Tangent
County Road
12°
100.4
Shed
26+31.8
42.3
78°12'
26+47.8
22+89.0

Cazadero

Level — Mar. 26-1913

| | | | | |
|---|---|---|---|---|
| B.M. | 7 432 | 107 432 | | |
| 0+00 | | | | 5 4 |
| 1 | | | | 6 6 |
| 2 | | | | 4 5 |
| 3 | | | | 4 1 |
| 4 | | | | 3 7 |
| T.P. | 6 120 | 110 01 | 3 512 | |
| 5 | | | | 5 7 |
| 6 | | | | 4 9 |
| +82 15 △ | | | | 6 0 |
| 7 | | | | 6 1 |
| +41 1 | | | | 4 8 |
| 8 | | | | 5 4 |
| 9 | | | | 6 0 |
| 10 | | | | 5 8 |
| T.P. | 4 77 | 109 00 | 5 910 | |
| 11 | | | | 4 6 |
| 12 | | | | 4 2 |
| B.M. | | | | 1 920 |
| 13 | | | | 3 9 |
| 14 | | | | 3 7 |
| +78 6 △ | | | | 3 8 |
| T.P. | 9 740 | 115 01 | 3 730 | |
| 15 | | | | 10 1 |
| +14 0 | | | | 9 6 |
| +23 5 | | | | 6 5 |

| | | |
|---|---|---|
| | | Elev 100.00 Ass'md. |
| 100.00 | Spik in | Cap. East End Bridge |
| 102.0 | Base Rail | (107.084) by Reardon |
| 100.8 | Ground. | |
| 102.9 | Base Rail | |
| 103.3 | " " | |
| 103.1 | " " | |
| 103.920 | T.P. | |
| 104.3 | Bass Rail | |
| 105.1 | | |
| 104.0 | Ground | |
| 103.9 | " | |
| 105.2 | ℄ Track | |
| 104.6 | Ground | |
| 104.0 | " | |
| 104.2 | ℄ Track | |
| | | |
| 104.23 | T.P. | |
| 104.4 | | |
| 105.8 | | |
| | | 114.134 |
| 107.08.0 | Spike in Stump at End of Depot | |
| 105.1 | ℄ Track | |
| 105.3 | " | |
| 105.2 | " | |
| 105.27 | T.P. | |
| 104.9 | | |

# Cazadero

## Levels. Mar 1913

| | | | | |
|---|---|---|---|---|
| 16 | | $115^{01}$ | | $6^{6}$ |
| T.P. | $9^{05}$ | $123^{68}$ | $0^{380}$ | |
| 17 | | | | $6^{9}$ |
| +21 △ | | | | $7^{3}$ |
| 18 | | | | $11^{4}$ |
| 19 | | | | $10^{7}$ |
| +82 | | | | $11^{0}$ |
| +86 Rock | | | | $2^{3}$ |
| 20 | | | | $+5^{1}$ |
| +03 △ | | | | $+5^{1}$ |
| +08 | | | | $+4^{8}$ |
| +15 | | | | $+3^{5}$ |
| T.P. | $3^{04}$ | $124^{39}$ | $2^{33}$ | |
| +17 | | | | $8^{8}$ |
| 21 | | | | $6^{2}$ |
| +64 | | | | $7^{8}$ |
| +76 | | | | $13^{0}$ |
| 22 | | | | $13^{8}$ |
| +27 | | | | $13^{7}$ |
| +30 | | | | $11^{8}$ |
| +38 | | | | $12^{0}$ |
| +42 | | | | $15^{0}$ |
| +48 △ | | | | $11^{0}$ |
| T.P. | $4^{77}$ | $118^{52}$ | $10^{64}$ | |
| +81 | | | | $4^{7}$ |
| +89 | | | | $8^{9}$ |
| 23 | | | | $9^{6}$ |

| | | | |
|---|---|---|---|
| 108 4 | | | |
| 114 630 | TP | | |
| 116 8 | | | |
| 116 4 | | | |
| 112 3 | | | |
| 113 0 | | | |
| 112 7 | foot of Rock | | |
| 121 4 | on Rock | | |
| 128 8 | | | |
| 128 8 | Top of Rock | | |
| 128 5 | on " | | |
| 127 2 | " " | | |
| 121 35 | T.P. | | |
| 115 6 | | | |
| 118 2 | | | |
| 116 6 | | | |
| 111 4 | | | |
| 110 6 | | | |
| 110 7 | | | |
| 112 6 | | | |
| 112 4 | | | |
| 109 4 | Creek | | |
| 113 4 | | | |
| 113 75 | T.P. | | |
| 113 8 | | | |
| 109 6 | | | |
| 108 9 | | | |

Cazadero.

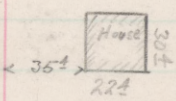
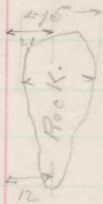
Mar. 26-1913

| | | | | |
|---|---|---|---|---|
| 24 | | 118 5/2 | | 9 1/- |
| T.P. | 5 68/- | 115 48/- | 8 72/- | |
| 25 | | | | 4 9/- |
| 26 | | | | 5 0/- |
| +17 8/- Δ | | | | 4 7/- |
| +31 8/- | | | | 4 7/- |
| BM. | | | 1 750/- | |

| | | | |
|---|---|---|---|
| $109\frac{4}{}$ | | | |
| $109\frac{80}{}$ | T.P. | | |
| $110\frac{6}{}$ | | | |
| $110\frac{5}{}$ | | | |
| $110\frac{8}{}$ | | | |
| $110\frac{8}{}$ | | | |
| $113\frac{730}{}$ | BM spik in curb at Corner of Shed. | | |

Cazadero

Mar. 26-1913

| | | | | |
|---|---|---|---|---|
| 9 | | Lt | | |
| 8 | | | | |
| 7 | | | | $\frac{\Phi}{18^2}$ $\frac{+1^1}{18^2}$ |
| | $+82^{15}$ Δ | | | $\frac{\Phi}{26^6}$ $\frac{+1^3}{26^6}$ |
| 6 | | | | $\frac{\Phi}{3^2}$ |
| | $+54^3$ |   | | |
| | $+16^7$ | End Spur. Rt. $38^7$ | | |
| 5 | | | | $\frac{fence}{50}$ |
| 4 | | | | |
| | $+72$ | Rt 21 |   | |
| | $+24^2$ | Rt. 12 | | |
| 3 | | | | $\frac{fence}{50}$ |
| 2 | | | | |
| 1 | | | | |
| 0+00 | | | | |

5 + 16
1 31
3 85

Ŧ = Cent. track
B.C. Bank Creek

℄ Pt.

$\frac{104^{0}}{00}$ $\frac{Ŧ}{11^{9}}$ $\frac{+0^{3}}{16^{0}}$ $\frac{-4^{6}}{30^{0}}$ $\frac{-8^{1}}{41}$

$\frac{104^{6}}{00}$ $\frac{+0^{3}}{18^{0}}$ $\frac{Ŧ}{14^{5}}$ $\frac{-7^{9}}{34}$ $\frac{B.C}{34}$

$\frac{103^{9}}{00}$ $\frac{-0^{5}}{8^{0}}$ $\frac{-4^{6}}{20}$ $\frac{B.C.}{20}$

$\frac{104^{0}}{00}$ $\frac{-5^{9}}{22}$ $\frac{B.C.}{22}$

$\frac{105^{1}}{00}$ $\frac{-2^{0}}{20}$ $\frac{-4^{8}}{72^{0}}$ $\frac{-9^{5}}{92^{0}}$ $\frac{B.C.}{92^{0}}$

$\frac{104^{3}}{00}$ $\frac{-1^{6}}{21}$ $\frac{Ŧ}{38^{7}}$ $\frac{-1^{6}}{73}$ $\frac{-5^{7}}{118}$ — $\frac{B.C.}{118}$

$\frac{103^{7}}{00}$ $\frac{-2^{4}}{22}$ $\frac{℄ Spur}{27^{8}}$ $\frac{-2^{1}}{112}$ $\frac{B.C}{112}$

$\frac{103^{3}}{00}$ $\frac{℄ Spur}{24^{7}}$ $\frac{-2^{8}}{48}$ $\frac{-2^{9}}{87}$ $\frac{B.C}{100}$ $\frac{-8^{4}}{100}$

$\frac{102^{9}}{00}$ $\frac{Ŧ}{3^{2}}$ $\frac{-0^{2}}{8^{5}}$ $\frac{-3^{0}}{27}$ $\frac{-2^{5}}{43}$ $\frac{-6^{8}}{46}$ $\frac{-7^{7}}{55}$ $\frac{B.C.}{56}$

$\frac{108}{00}$ $\frac{Ŧ+1^{6}}{13}$ $\frac{-1^{3}}{34}$ $\frac{B.C.}{34}$

$\frac{102}{00}$ $\frac{-7^{2}}{29}$ $\frac{Bank\ Cr.}{29}$

385
15
1925
385
5775

# Cazadero

| | | | | | | |
|---|---|---|---|---|---|---|
| 19 ✓ | | | | | $+10^{1}$ / 53 | $+5^{8}$ / 43 |
| 18 ✓ | | | | fence / 46 | $+11^{9}$ / 46 | $+10^{6}$ / $35^{5}$ |
| $17+21^{1}$ △ ✓ | | | | | $+7^{7}$ / 55 | $+6^{3}$ / 32 |
| 17 ✓ | | S.E.Cor. Church / 55 | | $-7^{2}$ / 55 | fence / 55 | $-5^{0}$ / 31 |
| 16 ✓ | | | | | $+8^{3}$ / 71 | West Lin O.R. / 71 |
| 15 ✓ | | | | | | $+7^{4}$ / 57 |
| $14+78^{6}$ △ ✓ | | | | | | |
| 14 ✓ | | | | | | |
| 13 ✓ | | | | | | |
| 12 ✓ | | | | | | |
| 11 ✓ | | | | | | |
| 10 ✓ | | | | | | |
| $9+65^{1}$ △ ✓ | | | | | | |

C.R. County Road
T.T. turntable.

| Lt | | | ℄ | | | Rt | | | |
|---|---|---|---|---|---|---|---|---|---|
| ℄ C.R. | | | | | | ← Gravel Bar. → | | | |
| +7° / 34 | +6° / 24 | +3⁴ / 20 | 113° / 00 | −2⁷ / 13° | −12² / 20 | −20⁷ / 51 | −16⁶ / 80 | −19⁴ / 138 | Edge Water / 138 |
| | | ℄ C.R. | | | | ← Gravel Bar. → | | | |
| +6° / 32 | +6⁸ / 22 | | 112³ / 00 | −4⁵ / 13° | −11⁵ / 23° | −16⁸ / 42° | −14⁷ / 85° | −19³ / 155 | Edge W / 155 |
| | | ℄ C.R. | | | | ← Gravel Bar. → | | | |
| +1⁶ / 26 | +2⁹ / 19 | | 116⁴ / 00 | −14° / 29° | −20⁶ / 40 | −17³ / 106 | −21³ / 166° | | Edge Water / 166° |
| −0⁸ / 27 | ℄ C.R. / 19 | | 116⁸ / 00 | −11⁷ / 33 | B.C. / 33 | | | | |
| ℄ C.R / 51 | +6⁴ / 51 | | 108⁴ / 00 | −3⁷ / 35 | Edge Pit T.T. / 35° | −7⁷ / 76 | B.C / 76 | | |
| +4⁵ / 19 | −0² / 7° | | 104⁹ / 00 | +0⁵ / 17° | −3⁵ / 55° | ℄ Spur −1⁸ / 75° | −0⁷ / 106° | | |
| | | | 105² / 00 | −3⁴ / 46 | −2² / 56⁵ | ℄ Spur / 56⁵ | −3⁴ / 71 | −2² / 107 | B.C. / 107 |
| | | | 105³ / 00 | −1⁹ / 48 | −4⁴ / 78 | −3⁹ / 144 | B.C / 144 | | |
| | | | 105¹ / 00 | −1² / 26° | −1° / 57° | −4⁷ / 108 | −5° / 140 | −2⁷ / 167 | B.C / 167 |
| | | | 105⁸ / 00 | −1¹ / 57 | −3⁹ / 76 | −4⁹ / 124 | B.C. / 124 | | |
| | | | 104⁴ / 00 | 00 / 9° | −1⁶ / 28 | −4⁸ / 41 | −7⁷ / 97° | B.C. / 97° | |
| | | | 104² / 00 | 00 / 7° | −5⁸ / 22 | −5⁴ / 55 | B.C. / 55 | | |
| | | | 104¹ / 00 | −0⁵ / 9° | −7¹ / 22 | −8⁴ / 42 | B.C. / 42 | | |

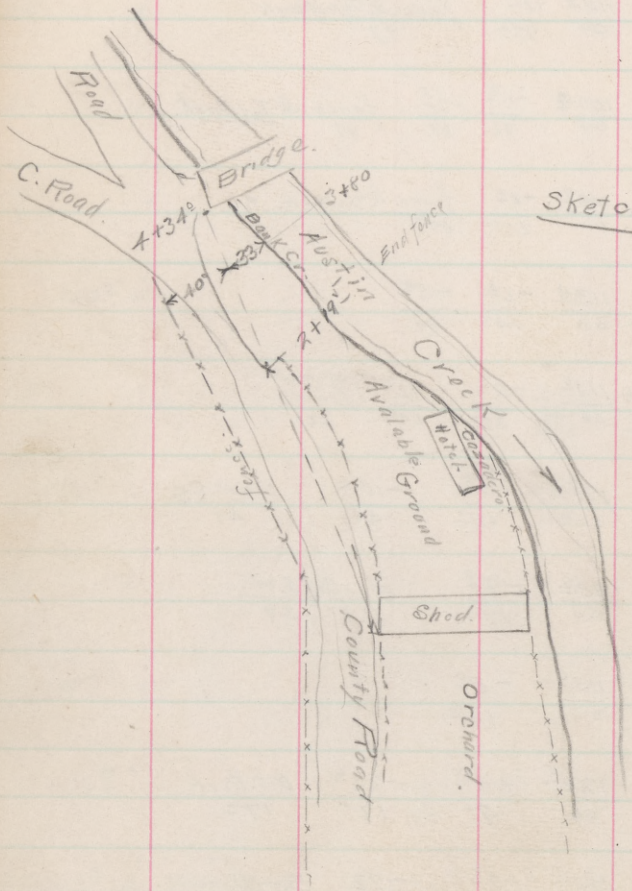
# Cazadero

Mar-26-1913

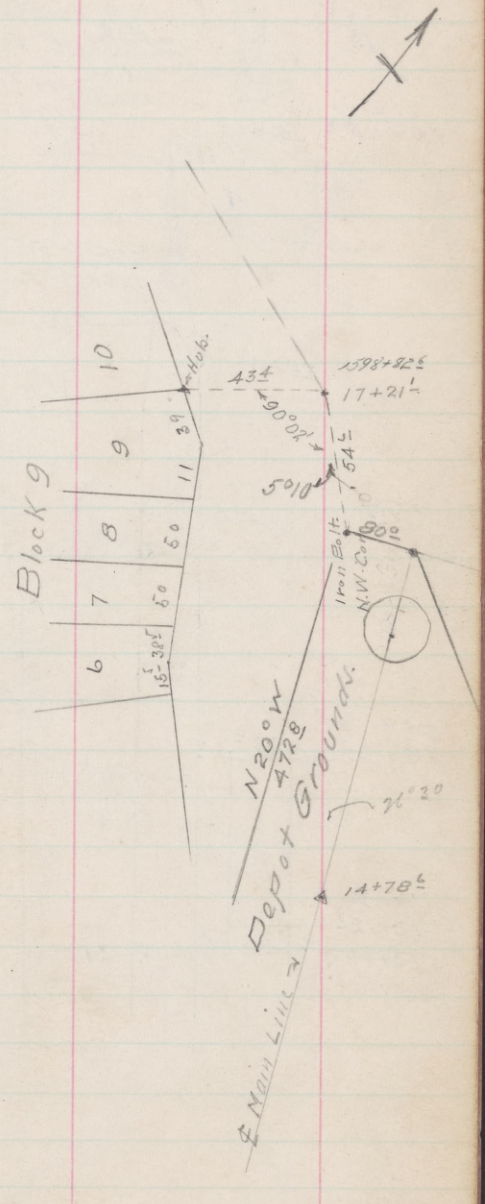
| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| | +31$^{8}$ | | | | | | | |
| 26 | ✓ | | | | | | | |
| 25 | ✓ | | | | | | | |
| 24 | ✓ | | | | | | | East Side orchard |
| 23 | ✓ | | | | | | | |
| | +48$^{7}$ ✓ ⚓ | | | | | | fence 30$^{5}$ | −0$^{8}$ / 30$^{5}$ |
| 22 | ✓ | | | | | fence 47$^{0}$ | +7$^{3}$ / 47$^{0}$ | +3$^{3}$ / 30 |
| | +76$^{0}$ ✓ | | | | | +6$^{8}$ / 46 | +5$^{0}$ / 32 | −0$^{1}$ / 24 |
| 21 | ✓ | | | | fence 52 | +10$^{0}$ / 52 | +7$^{5}$ / 33 | +1$^{3}$ / 26$^{0}$ |
| | | | | | | ← Rock | | → |
| | +17$^{0}$ ✓ | | | | fence 47 | +12$^{7}$ / 47 | +9$^{5}$ / 32 | +5$^{2}$ / 30 |
| | +08$^{3}$ ✓ | | | −2$^{2}$ / 50 | −3$^{6}$ / 40 | −7$^{4}$ / 35 | ℄ C.R. −7$^{0}$ / 28 | |
| 20 | +03$^{3}$ ✓ ⚓ | Top Rock | fence 50 | −2$^{0}$ / 50 | −3$^{5}$ / 40 | −7$^{4}$ / 34 | ℄ C.R. −6$^{8}$ / 28 | Bot. Rock −7$^{4}$ / 17 |
| 19 | +86 ✓ | foot of Rock | | | | fence 53 | +10$^{4}$ / 53 | +7$^{0}$ / 41 |

| Lt | | ℄ | | | Rt |
|---|---|---|---|---|---|
| Corner Bold. fence. 42 | +1° 42 | 110⁸ 00 | −1⁷ 70⁵ | | fence & Top Bank. 70⁵ |
| fence 44° | +0⁸ 44 | 110⁵ 00 | −1¹ 83 | | fence & Top Bank. 83⁴ |
| fence. 40 | +0⁷ 40 | 110⁶ 00 | −1⁷ 97° | | fence & Top Bank 97 |
| Co Road. fence 27 | −1⁴ 27 | 109⁴ 00 | −1³ 76 | −2⁵ 81 | fence & Top Bank. 81 |
| +1¹ 36 | orchard. fence 36 | 108⁹ 00 | −1¹ 69° | | fence & Top Bank. 69⁵ |
| −2° 15⁵ | +1° 7⁵ | 113⁴ 00 | −6° 14° | −5° 80 | |
| ℄ Road +5° 20 | +3⁷ 11° | 110⁶ 00 | −2⁶ 39° | −12³ 63° | orchard fence 63° |
| ℄ Road +0⁸ 16° | | 111⁴ 00 | fence −5³ 18° | −10⁶ 49 | Bank. Cr. 49 |
| ℄ Road +2¹ 18° | +2¹ 7° | 118² 00 | −9⁹ 19° | | Ban Cr. 19° E.W. 39 |
| ℄ Road +6¹ 23 | +4⁷ 14 | 115⁶ 00 | −8° 19° | | |
| −4⁵ 15 | −2° 7° | 128⁵ 00 | −0⁸ 7° | −23° 17° | Bot. Rock 17° |
| −4⁴ 15 | −3⁸ 7° | 128⁸ 00 | −0⁷ 8 | −22 18 | Bot Rock 18 |
| ℄ C.R. +8° 33 | +6⁶ 25 | 121⁴ 00 | −6° 21° | −14° 28 | Edge Gravel Bar 30 |

Cazadero. Mar. 26-1913

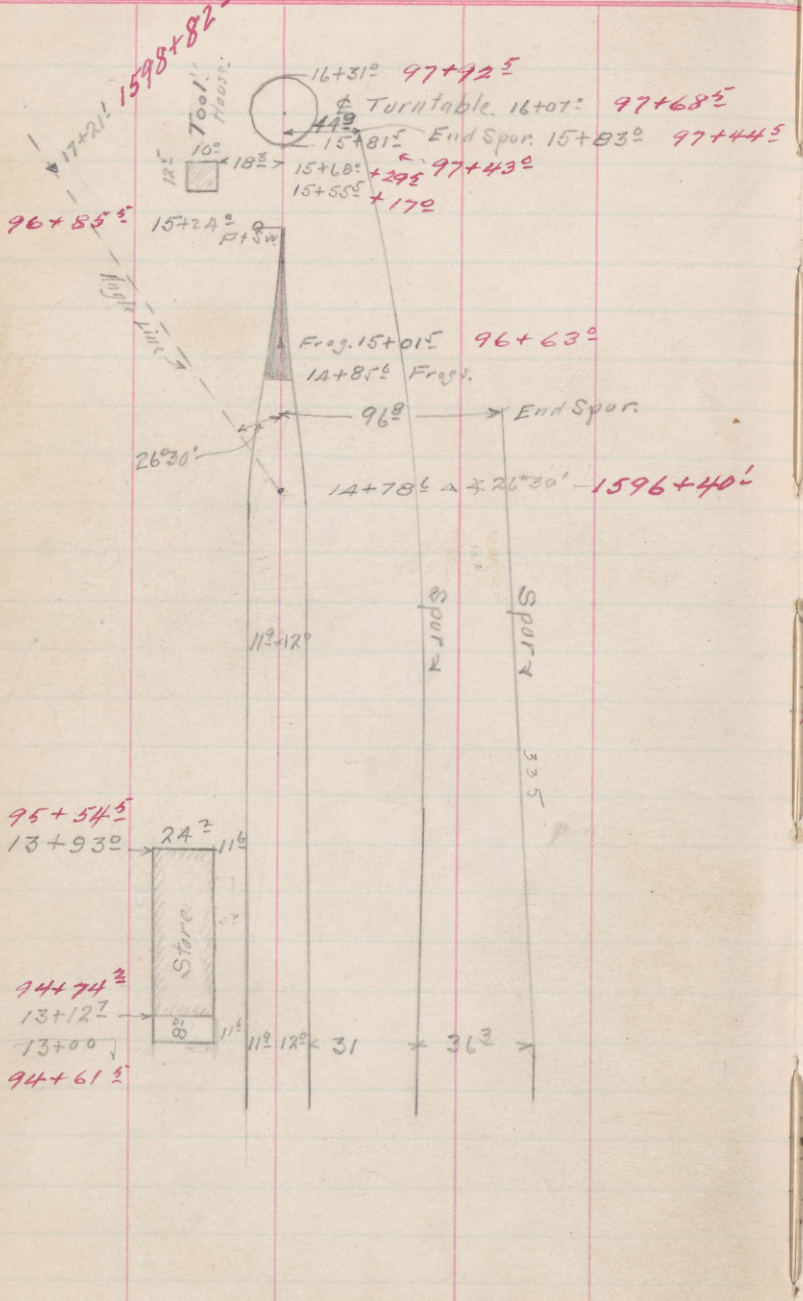


Mar-27-1913


Block 9
10
9
8
7
6
11
39
50
50
15-38
Hob.
43
90°02'
1598+82
17+21
54
5°10'
80°
Iron Bolt
N.W. Cor
N20°W
4728
Depot Grounds.
14+78
℄ Main Line

# Cazadero

Mar. 27-1913



1913

B.S Shop { $12+43^{7}$ P.I. / $12+33^{0}$ R.A.

($1593+74^{4}$) → $12+12^{9}$

$93+61^{5}$ 12+00

$93+47^{5}$ Frog. $11+81^{0}$

$93+23^{5}$ P.I. $11+62^{0}$

$+22^{0}$ P+Sw. $34^{1}$ R $11+60^{5}$

$93+13^{0}$ R.A. $11+51^{5}$

$92+92^{0}$ R.A. ℄ Schute $11+30^{5}$

$+42^{7}$ / $26^{9}$ → Frog. $10+81^{2}$

$92+26^{9}$ Frog $10+65^{4}$

$+38^{9}$ { $10+77^{4}$ P.I.

$+32^{0}$ $10+70^{5}$ Buld

$+04^{5}$ $10+43^{0}$ P.t Sw.

$91+59^{0}$

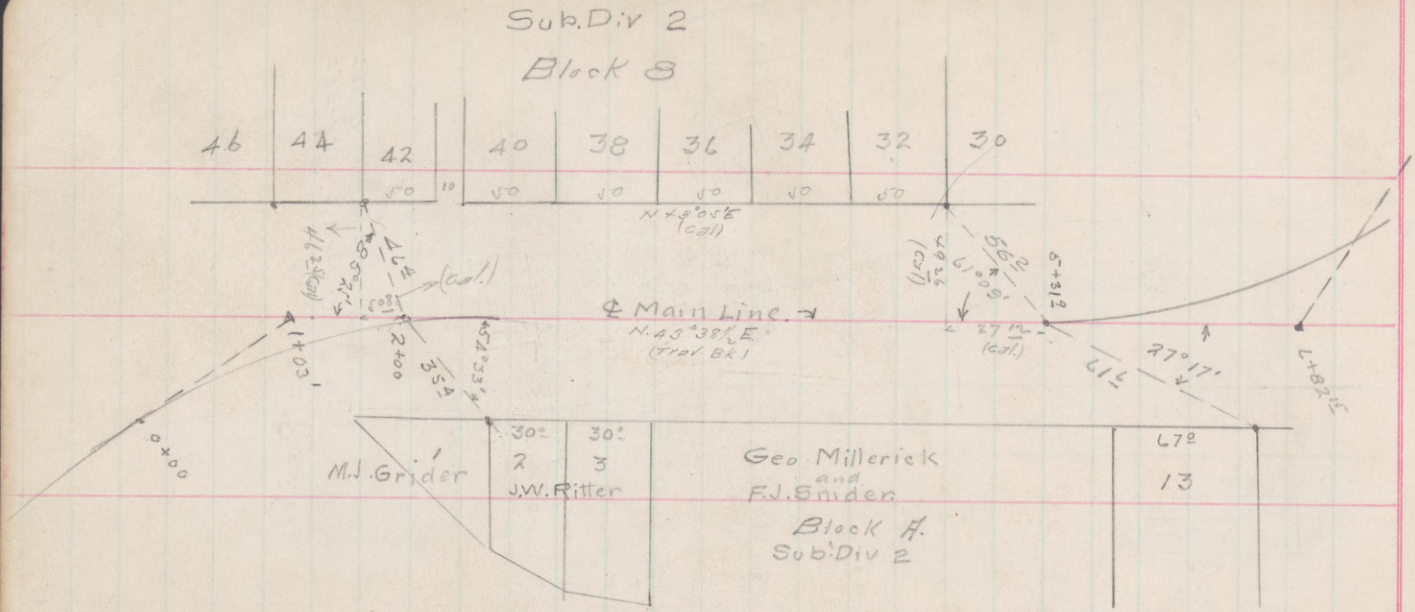
Frog $9+97^{5}$

Lead $33^{8}$

$9+65^{1}$ Δ 10°50' $91+26^{6}$

$9+63^{7}$ P+Sw. $91+25^{2}$

10°50'




Cazadero

Nov 27-1913

Sub. Div. 2

Block 8

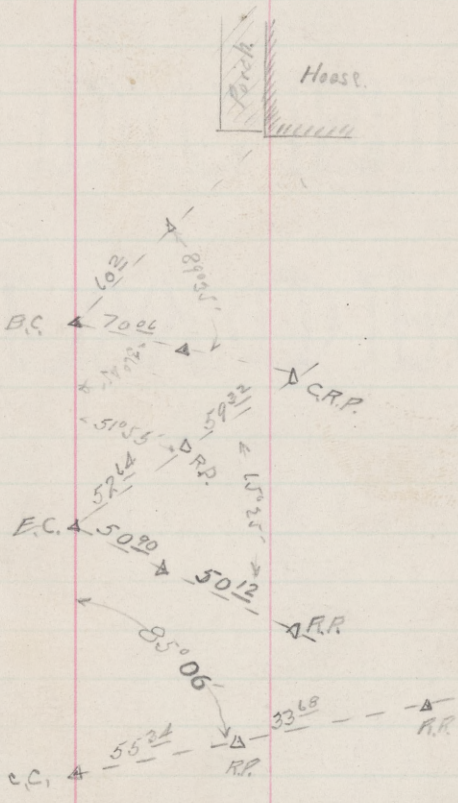
# MARKHAM. Branch.

April 25-1913

| | | | |
|---|---|---|---|
| 1327+82.77 C.C.T 2 7/8 △ | | 6°33' | |
| +50 | △ 13°24' | 4°65' | T △ 19°06' |
| 1327+00 | | 2°25' | St+t = 9[illegible] |
| | | 0°00' | |
| 1326+51.77 C.C. 10° L+△ | | 1°07½' | |
| +31.77 | △ 3°00' | 0°42 | |
| +21.77 | L.C. 60.00 | 0°22½ | |
| 1326+01.77 | | 0°09 | |
| 1325+91.77 B.C.T-2 7/8 △ | | 0°00 | |
| +50 | | | |
| 1325 | | | |
| +50 | | | |
| 1324+05.13 E.C. △ | | 3°33 3/4 | |
| +90.13 | △ 3°33 3/4 | 3°05 5/8 | |
| +75.13 | | 2°30 | |
| +60.13 | | 1°46 7/8 | |
| +45.13 | | 0°56 1/4 | |
| +30.13 C.C. 14° △ | | 0°00 | |
| | | 10°27' | |
| 1323 | | 8°11½ | T △ 32°09' |
| +50 | △ 20°54' | 4°26½ | St+t = 106.09 |
| 1322 | | 0°41½ | |
| 1321+90.8 C.C. 15° Rt. | | 2°03¾ | |
| +75.8 | | 1°24 3/8 | |
| +60.8 | △ 5°37½ | 0°52½ | |
| +45.8 | L.C. 74.97 | 0°28 1/8 | |
| +30.8 | | 0°11¼ | |
| 1321+15.8 B.C. T 4 86/2 | | 0°00 | |

1321+12.94 (J.E. Williams) tang produced 9± from B.C. 1321+03.74

19°08
9°33'
19°06

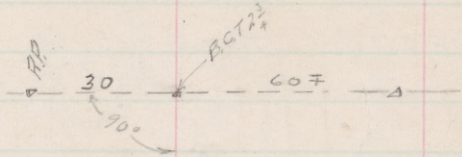


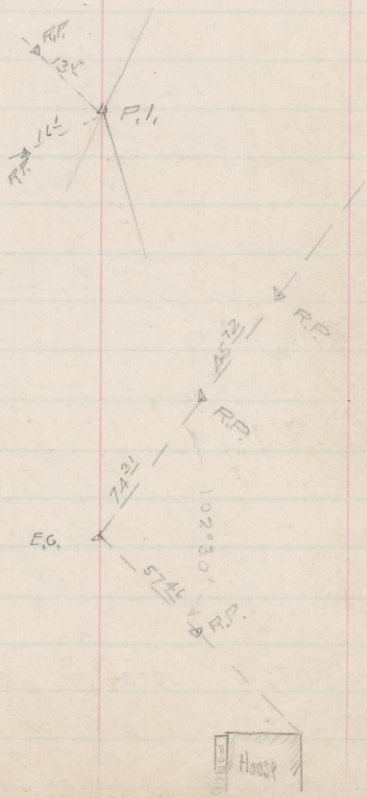
# MARKHAM Branch.

50
105
36.5

April 26/13

| | | | |
|---|---|---|---|
| 1336 | 9°19½ | ✓ | |
| +50 | 6°49½ | ✓ | Δ 39°18 |
| 1335 | 4°19½ | ✓ | St+L = 265 16 |
| +50 | 1°49½ | ✓ | |
| 1334 +13½ C.C. 10° Lt | 0000 2°06½ | ✓ | |
| +83½ | 1°24' | ✓ | × |
| +53½ | 0°45 | ✓ | |
| 1333 +23½ | 0°18' | ✓ | |
| 1332+93½ B.C. T-2¾ | | ✓ | |
| 1332+60 20 P.O.T. | 17 28 | ✓ | |
| 1332+61 28 =P.O.T. | | ✓ | |
| +50 | | ✓ | |
| +17 34 E.C. | 3°48½ | ✓ | |
| 1332 | 3°33 | ✓ | |
| +50 | 2°48 | ✓ | Δ 7°37' |
| 1331 | 2°03 | ✓ | St+127 43 |
| +50 | 1°18 | ✓ | |
| 1330 | 0°33' | ✓ | |
| 1329+63 45 B.C. 3° Rt | | ✓ | |
| +50 | | | |
| 1329 | | | |
| +50 | | | |
| 1328+42 77 E.C. | 1°52½ | ✓ | |
| +27 77 | 1°33 | ✓ | |
| 1328+12 77 | 1°07½ | ✓ | |
| +97 77 Δ 3000 | 0°36 | ✓ | |
| 1327+82 77 C.C. T 2½- | 0°00 | ✓ | |


R.P.
B.C.T 2 3/4
30
60 F
90°


R.P.
13 5
P.I.
16 1/2
R.P.
R.P.
45 72
R.P.
74 31
E.G.
102°30'
57 46
R.P.
House

# MARKHAM Branch

6°00'
2°15'
3°45'

April -1913

| | | | | |
|---|---|---|---|---|
| +50 | | 0°38 | ✓ | |
| | | 0°00' | | |
| 1346+40.9 | C.C. 14° R.T. | 4°33' ✓ | ✓ | 2305 |
| 1346+10.9 | | 3°18 | ✓ | R.P. |
| +80.9 | | 2°15 | ✓ | 2862 |
| +50.9 | Δ 12°36' 17963 L.C. | 1°24' | ✓ | |
| 1345+20.9 | | 0°45 | ✓ | |
| +90.9 | | 0°18 | ✓ | |
| 1344+60.9 | B.C. T 2 3/4 | | ✓ | |
| +50 | | | ✓ | |
| 1344 | | | ✓ | |
| +50 Δ | R.O.T. | ✓ | | |
| 1343 | | ✓ | | |
| +50 | | ✓ | | |
| 1342 | | ✓ | | |
| +50 | | ✓ | | |
| 1341 | | ✓ | | |
| +50 | | ✓ | | |
| 1340 | | ✓ | | |
| +60 | | ✓ | | |
| 1339 +90 | | ✓ | | |
| +50 | | ✓ | | |
| 1338+06.5 | E.C. | ✓ | | |
| +76.5 | | | | |
| +46.5 | | | | |
| 1337+16.5 | | | | |
| 1336+86.5 | C.C. T 2 3/4 | 13°39' | | |
| 1336+50 | | 11°49.5 | | |

46+40.9
1344+60.9
1+80.0

P.O.T.
R.P.
Spike in root of
Baytree
52° 30'
R.P.
84° 30'
B.C.T.
R.P.
River

Fence Cor.
24°
75°
30°
49°20'
67°20'
R.P.
Rock

# MARKHAM Branch.

See Page 38.

| | | | | | |
|---|---|---|---|---|---|
| 9+56$^{56}$ | P.O.T. | | | | |
| 1355+44$^{53}$ | E.C = | | ✓ | ✓ | |
| 1355+14$^{53}$ | | | ✓ | ✓ | |
| +84$^{53}$ | △ 6°00' | | ✓ | ✓ | |
| +54$^{53}$ | | | ✓ | ✓ | |
| +24$^{53}$ | C.C. T 2¾ | 0°00' | ✓ | ✓ | |
| 1354 | | 1°13½ | ✓ | ✓ | |
| +50 | | 3°43½ | ✓ | ✓ | |
| 1353 | | 6°13½ | ✓ | ✓ | 18°31' |
| +50 | | 8°43½ | ✓ | ✓ | |
| +39$^{4}$ | C.C. 10° | 9°15½ | ✓ | ✓ | |
| 1352 | | 1°47' | ✓ | ✓ | |
| +50 | △ 13°58' | 4°03' | ✓ | ✓ | (1351+87$^{6}$ End Br.) |
| 1351 | | 6°19' | ✓ | ✓ | (1351+40$^{2}$ Beg Br.) |
| ~~1351+~~ | | | | | |
| 1350+85$^{4}$ | C.C. 9°04' | 6°59<br>0°00' | ✓ | ✓ | 31°07 |
| +50 | | 2°29' | ✓ | ✓ | 28°38 |
| 1350 | | 5°59' | ✓ | ✓ | 25°08 ✓ |
| +50 | | 9°29' | ✓ | ✓ | 21°38 ✓ |
| 1349 | | 12°59 | ✓ | ✓ | 18°08 ✓ |
| +50 △ | △ 62°14' | 16°29 | ✓ | ✓ | 14°38 ✓ |
| 1348 | | 19°59' | ✓ | ✓ | 11°08 ✓ |
| +50 △ | | 23°29'<br>7°38 | ✓ | ✓ | 7°38 |
| B47 | | 4°08 | ✓ | ✓ | |

St+t = 401$^{85}$ P.I. to B.C.
St = 317$^{83}$ P.I. to C.C.

619
39
658

40/60
0.06

240
02
2.72

52+39.4
50+85.4
154.0

$1 = \frac{100 \times a}{D}$

154 × 9.07
0.77

6349
6349
6.9839

9713
4077
5636

6.93
60
55.80

59.114
2364
591
8.274
4.137
60
8.220

4°08'

$\frac{14 \times 50}{100} = 7$ 3°30'

47+00.0
46+40.9
59.1

℄ of Pres. Track.

1+90 ✓

1+75 ✓

1+61 ✓

1+48 ✓

1+35 ✓

1+21 ✓

1+08 ✓

0+94 ✓

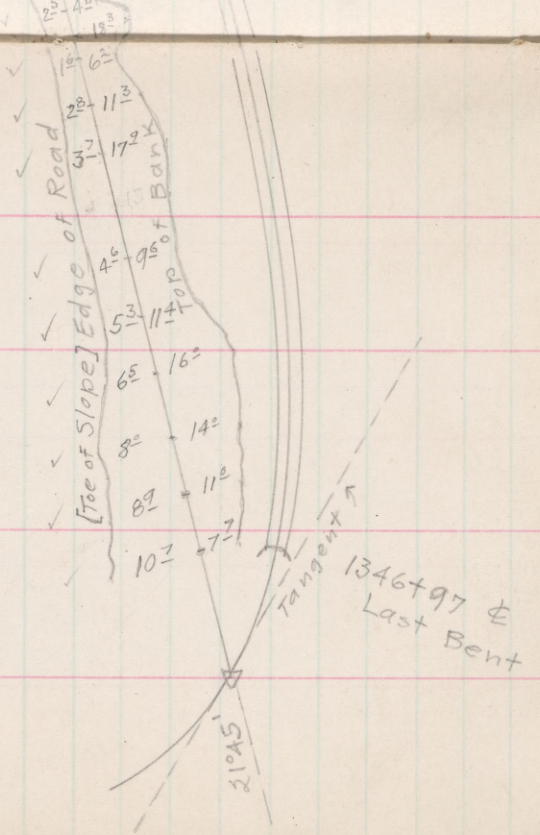
0+80 ✓

0+67 ✓

0+52 ✓

1347+50

0+00



(28)

Markham, March 4th-14

4+04.4 = 1343+16.3 ±

3+57.0 ±

1343+92.5 ℄ 1st Bent

3+20.7 ✓

3+06.2 ✓

2+94.7 ✓

2+87.9

2+73.3 ✓

2+58.7 ✓

2+45.2 ✓

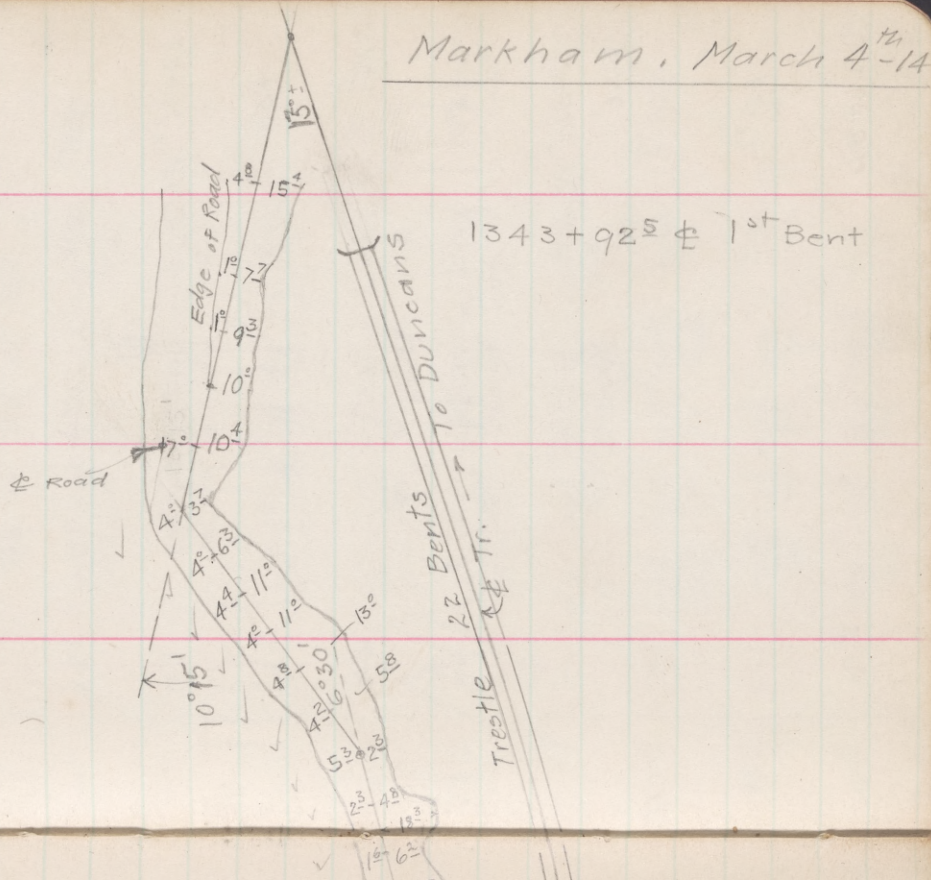
2+33.1 ✓

2+19.5 ✓

2+08.0 ✓

1+89.9 ✓

1+75.1 ✓



# Markham Br.

## Cross Sections.

Apr. 1918

| Station | Elev. | Grade | Cut | Fill. |
|---|---|---|---|---|
| 1322 | $20\frac{7}{}$ | $20\frac{7}{}$ | — | — |
| 1322+50 | $20\frac{0}{}$ | $20\frac{4\,8}{}$ | | |
| 1322+62 | $20\frac{4\,3}{}$ | $20\frac{4\,3}{}$ | | |
| 1323 | $22\frac{0\,0}{}$ | $20\frac{2\,7\,5}{}$ | | |
| +30 $\frac{13}{}$ C.C. | $22\frac{4}{}$ | $20\frac{1\,4\,7}{}$ | | |
| +60 $\frac{13}{}$ | $21\frac{2}{}$ | $20\frac{0\,2}{}$ | | |
| 1324+05 $\frac{13}{}$ E.C. | $20\frac{9}{}$ | $19\frac{8\,1}{}$ | | |
| +50 | $19\frac{6}{}$ | $19\frac{6\,3\,7}{}$ | | |
| 1325 | $18\frac{2}{}$ | $19\frac{4\,2\,5}{}$ | | |
| +50 | $16\frac{6}{}$ | $19\frac{2\,1\,2}{}$ | | |
| 1325+91 $\frac{77}{}$ P.C. | $16\frac{4}{}$ | $19\frac{0\,3\,5}{}$ | | |
| 1326 | | $\times 19\frac{0\,0\,0}{}$ | | |
| +21 $\frac{77}{}$ | $17\frac{6}{}$ | | | |
| +51 $\frac{77}{}$ | $18\frac{3}{}$ | | | |
| 1326+80 | | | | |

$-0\frac{4\,2\,5}{}$

Level.

| Area | Left. | | | | ℄ | | | | Rt |
|---|---|---|---|---|---|---|---|---|---|
| ~~0~~ | + $5^{0}$ | $+0^{5}$ / $9^{7}$ | $+0^{5}$ / $9^{0}$ | $\frac{00}{00}$ | $\frac{00}{3^{6}}$ | $+1^{3}$ / $9^{0}$ | $+1^{3}$ / $10^{9}$ | | |
| $2^{7}$ | $17^{0}$ | $+1^{3}$ / $12$ | $+0^{9}$ / $10$ | $\frac{00}{8^{0}}$ | $-0^{5}$ / $00$ | $\frac{00}{3^{0}}$ | $+2^{2}$ / $6^{0}$ | $+2^{2}$ / $10$ | $+2^{2}$ / $13^{0}$ |
| — | $19^{6}$ | | | $\frac{00}{10^{0}}$ | $\frac{00}{00}$ | $+1^{9}$ / $2^{6}$ | $+1^{9}$ / $10$ | $+2^{2}$ / $13^{0}$ | |
| $1^{4}$ | $30^{9}$ | $-0^{7}$ / $10^{0}$ | $\frac{00}{6^{0}}$ | $+1^{7}$ / $00$ | $+2^{4}$ / $10$ | $+2^{4}$ / $13^{6}$ | | | |
| — | $43^{9}$ | $+0^{8}$ / $11^{2}$ | $+1^{1}$ / $10$ | $+2^{2}$ / $00$ | $+2^{4}$ / $10$ | $+2^{2}$ / $13^{3}$ | | | |
| — | $28^{3}$ | $+0^{8}$ / $11^{2}$ | $+0^{8}$ / $10$ | $+1^{2}$ / $00$ | $+1^{9}$ / $10$ | $+1^{9}$ / $11^{9}$ | | | |
| — | $23$ | $+0^{4}$ / $10^{6}$ | $+0^{4}$ / $10^{0}$ | $+1^{1}$ / $00$ | $+1^{5}$ / $10$ | $+1^{9}$ / $12^{8}$ | | | |
| $1^{1}$ | $2^{7}$ | $-0^{4}$ / $9^{6}$ | $-0^{5}$ / $9^{0}$ | $\frac{00}{5^{0}}$ | $\frac{00}{00}$ | $+0^{5}$ / $10$ | $+0^{5}$ / $10^{7}$ | | |
| $27^{5}$ | ~~00~~ | $-2^{3}$ / $12^{4}$ | $-1^{9}$ / $9^{0}$ | $-1^{2}$ / $00$ | $-0^{8}$ / $9^{0}$ | $-0^{7}$ / $10^{1}$ | | | |
| $55^{4}$ | — | $-3^{3}$ / $13^{9}$ | $-3^{0}$ / $9^{0}$ | $-2^{6}$ / $00$ | $-2^{0}$ / $9^{0}$ | $-2^{3}$ / $12^{4}$ | | | |
| $57^{8}$ | — | $-2^{8}$ / $13^{2}$ | $-2^{8}$ / $9^{0}$ | $-2^{8}$ / $00$ | $-2^{1}$ / $9^{0}$ | $-2^{2}$ / $13^{3}$ | | | |
| $27^{4}$ | — | $-1^{9}$ / $11^{8}$ | $-1^{8}$ / $9^{0}$ | $-1^{4}$ / $00$ | $-0^{8}$ / $9^{0}$ | $-0^{8}$ / $10^{2}$ | | | |
| $13^{0}$ | $00$ | $-1^{4}$ / $11^{1}$ | $-1^{2}$ / $9^{0}$ | $-0^{7}$ / $00$ | $\frac{00}{9^{0}}$ | | | | |
| $4^{1}$ | $5^{2}$ | $-0^{9}$ / $10^{2}$ | $-0^{8}$ / $9^{0}$ | $\frac{00}{00}$ | $+0^{9}$ / $10$ | $+1^{0}$ / $11^{5}$ | | | |

| Station | Elev | Grade | Cut | Fill |
|---|---|---|---|---|
| 1327 | 20 3 | 19 00 | | |
| 2X2 Box | 25 ft. | | | |
| 1327 +45 | | | | |
| 1327+50 | 18 8 | | | |
| +82 77 66 | 18 1 | | | |
| 1328 +12 77 | 17 1 | | | |
| +42 77 E.C | 16 7 | | | |
| +50 | | | | |
| +84 - 2X1 Box | | 35 = 1-18 1-24 | | |
| 1329 | 16 1 | Level | | |
| +50 | 17 1 | | | |
| 1330 | 17 2 | | | |
| +32 | 19 2 | | | |
| +50 | 19 2 | | | |
| 1331 | 22 2 | | | |
| +50 | 21 3 | 19 00 | | |

| | Lt | C | Rt. |
|---|---|---|---|
| 00 | $13^{\circ}$ | $\frac{00}{10}$ $\quad +1\frac{3}{00}$ | $\frac{00}{10}$ |
| $8^{\circ}$ | $5^{5}$ | $\frac{-1^{2}}{10^{8}}$ $\frac{-1^{\circ}}{9^{\circ}}$ $\frac{00}{00}$ $+1\frac{3}{10}$ $+1\frac{5}{12^{2}}$ | |
| $7^{8}$ | $10^{6}$ | $\frac{-1^{4}}{11^{2}}$ $\frac{-1^{2}}{9^{\circ}}$ $\frac{-0^{2}}{00}$ $\frac{00}{1^{\circ}}$ $+1\frac{7}{10}$ | $+1\frac{7}{12^{5}}$ |
| $27^{4}$ | 00 | $\frac{-2^{8}}{13^{2}}$ $\frac{-2^{4}}{9^{\circ}}$ $\frac{-0^{9}}{00}$ $\frac{-0^{4}}{9^{\circ}}$ $\frac{-0^{4}}{9^{6}}$ | |
| $50^{\circ}$ | — | $\frac{-3^{8}}{14^{7}}$ $\frac{-3^{4}}{9^{\circ}}$ $\frac{-1^{9}}{00}$ $\frac{-1^{5}}{9^{\circ}}$ $\frac{-1^{1}}{10^{2}}$ | |
| $55^{3}$ | — | $\frac{-4^{1}}{15^{1}}$ $\frac{-3^{2}}{9^{\circ}}$ $\frac{-2^{3}}{00}$ $\frac{-1^{7}}{9^{\circ}}$ $\frac{-1^{5}}{11^{2}}$ $\left(\frac{+0^{8}}{18}\right.$ | $\left.\frac{+4^{1}}{55}\right)$ |
| $53^{7}$ | — | $\frac{-4^{\circ}}{15^{\circ}}$ $\frac{-3^{1}}{9^{\circ}}$ $\frac{-2^{2}}{00}$ $\frac{-1^{7}}{9^{\circ}}$ $\frac{-1^{5}}{11^{2}}$ | |
| $76^{2}$ | — | $\frac{-5^{\circ}}{16^{5}}$ $\frac{-3^{7}}{9^{\circ}}$ $\frac{-2^{9}}{00}$ $\frac{-2^{6}}{9^{\circ}}$ $\frac{-2^{7}}{13^{1}}$ $\left(\frac{00}{17}\right.$ | $\left.\frac{+5^{2}}{55}\right)$ |
| $56^{7}$ | — | $\frac{-5^{2}}{16^{8}}$ $\frac{-3^{4}}{9^{\circ}}$ $\frac{-1^{9}}{00}$ $\frac{-1^{3}}{9^{\circ}}$ $\frac{-1^{6}}{11^{4}}$ $\left(\frac{00}{14}\right.$ | $\left.\frac{+12^{9}}{55}\right)$ |
| $66^{8}$ | — | $\frac{-6^{\circ}}{18^{9}}$ $\frac{-5^{4}}{9^{\circ}}$ $\frac{-2^{\circ}}{00}$ $\frac{-0^{7}}{2^{9}}$ $\frac{-0^{7}}{9^{\circ}}$ $\frac{-0^{5}}{9^{7}}$ $\left(\frac{00}{13}\right.$ $\frac{+6^{2}}{21^{7}}$ | $\left.\frac{+17^{3}}{55}\right)$ |
| $32^{9}$ | 00 | $\frac{-6^{1}}{18^{1}}$ $\frac{-3^{6}}{9^{2}}$ $\frac{00}{3^{\circ}}$ $\frac{00}{00}$ $\frac{00}{9^{\circ}}$ | |
| $15^{3}$ | $18^{3}$ | $\frac{-5^{2}}{16^{8}}$ $\frac{-1^{5}}{9^{\circ}}$ $\frac{00}{6^{\circ}}$ $\frac{+0^{2}}{00}$ $\frac{00}{6^{7}}$ $\frac{+2^{2}}{10}$ $\frac{+6^{3}}{16^{3}}$ $\left(\frac{+9^{7}}{20}\right.$ | $\left.\frac{+23}{56}\right)$ |
| 00 | $157^{8}$ | $\frac{+1^{1}}{11^{6}}$ $\frac{+1^{6}}{10}$ $+1^{2}$ $\frac{+3^{4}}{3^{\circ}}$ $\frac{+5^{3}}{00}$ $\frac{+9^{2}}{4}$ $\frac{+14^{6}}{15}$ $\frac{+20}{24^{6}}$ | $\frac{+27^{8}}{35}$ $\frac{+27^{8}}{55}$ |
| $14^{5}$ | $125\frac{46}{}$ | $\frac{-2^{3}}{12^{4}}$ $\frac{-2^{3}}{9^{\circ}}$ $\frac{-2^{\circ}}{5^{2}}$ $\frac{00}{3^{\circ}}$ $\frac{+2^{3}}{00}$ $\frac{+84}{10}$ $\frac{+10^{2}}{15}$ $\frac{+13^{3}}{23^{3}}$ | $\frac{+20^{2}}{39}$ $\frac{+25^{7}}{55}$ |

| Station | Elev. | Grade | Cut | Fill | | |
|---|---|---|---|---|---|---|
| 1332 | 19.2 | 19.0 | | | X | 7 |
| 1332+50 | 21.2 | | | | X | 5 |
| +60.2 | | | | | X | 4 |
| +74.6 | 19.0 | | | | X | 1 |
| +93.5 BC | 17.2 | | | | 61.5 | 1 |
| 1333+03.5 | | | | | 59.2 | 1 |
| +23.5 | 12.6 | | | | | |
| +53.5 | 12.6 | Level. | | | 116.8 | |
| | 1-Box 1x2"-36' 1-1x2-18 | | | | 165.7 | 1 |
| +83.5 | 13.5 | | | | 138.4 | |
| 1334+13.6 CC | 14.2 | | | | 71.2 | |
| +39 | 19.0 | | | | 39.7 | 3 |
| +50 | | | | | 19.6 | 5 |
| +73 | 19.0 | | | | 0.8 | |
| | 1-Box 1x2=72'-1-1x2'12 | | | | | |
| 1335 | 19.4 | | | | 12.9 | 3 |

| | Lt. | | | | ℄ | | | Rt. | |
|---|---|---|---|---|---|---|---|---|---|
| $75^{2}$ | $-5^{2}$ / $17^{8}$ | $-5^{2}$ / $13^{8}$ | $-5^{7}$ / $9^{0}$ | $00$ / $0^{5}$ | $+0^{2}$ / $00$ | $+6^{1}$ / $10^{0}$ | $+7^{9}$ / $15$ | $+9^{1}$ / $19^{1}$ | $+18^{5}$ / $55$ |
| $57^{3}$ | $-5^{6}$ / $17^{4}$ | $-5^{1}$ / $15^{0}$ | $-0^{5}$ / $9^{0}$ | $00$ / $7^{5}$ | $+2^{2}$ / $00$ | $+5^{0}$ / $10^{0}$ | $+7^{0}$ / $17$ | $+17^{6}$ / $55$ | |
| $45^{0}$ | $-6^{0}$ / $18^{0}$ | $-5^{4}$ / $14^{5}$ | $-2^{0}$ / $9^{0}$ | $00$ / $4^{0}$ | $+1^{3}$ / $00$ | $+4^{2}$ / $10$ | $+5^{9}$ / $15^{9}$ | | |
| $18^{9}$ | | $-4^{7}$ / $16^{1}$ | $-6^{0}$ / $12^{5}$ | $-2^{4}$ / $9^{0}$ | $00$ / $00$ | $+2^{7}$ / $10$ | $+3^{5}$ / $13^{5}$ | | |
| $1^{1}$ | ✓ | $-6^{0}$ / $18$ | $-6^{2}$ / $9^{0}$ | $-2^{3}$ / $5^{0}$ | $-1^{8}$ / $00$ | $00$ / $7^{5}$ | $+0^{7}$ / $10$ | $+0^{7}$ / $10^{7}$ | $+16^{0}$ / $55$ |
| $15^{0}$ | ✓ | $-6^{0}$ / $18$ | $-6^{2}$ / $9^{0}$ | $-6^{1}$ / $6^{0}$ | $-3^{0}$ / $00$ | $00$ / $10$ | | | |
| — | ✓ | $-5^{4}$ / $17^{1}$ | $-5^{0}$ / $9^{0}$ | $-6^{4}$ / $00$ | $-2^{8}$ / $9^{0}$ | $-1^{5}$ / $11^{3}$ | $00$ / $17^{0}$ | $+13^{5}$ / $55$ | |
| — | ✓ | $-6^{3}$ / $18^{4}$ | $-6^{3}$ / $9^{0}$ | $-6^{4}$ / $00$ | $-6^{2}$ / $9^{0}$ | $-5^{2}$ / $16^{8}$ | $00$ / $30$ | $+9^{3}$ / $55$ | |
| — | ✓ | $-5^{7}$ / $17^{5}$ | $-5^{7}$ / $9^{0}$ | $-5^{5}$ / $00$ | $-4^{7}$ / $9^{0}$ | $-4^{0}$ / $15^{0}$ | $00$ / $25^{8}$ | $+8^{4}$ / $55$ | |
| $1^{0}$ | ✓ | $-4^{7}$ / $16^{0}$ | $-4^{2}$ / $9^{0}$ | $-4^{1}$ / $00$ | $00$ / $8^{8}$ | $+0^{5}$ / $10$ | $+0^{5}$ / $10^{5}$ | $+7^{8}$ / $55$ | |
| $30^{6}$ | ✓ | $-4^{3}$ / $15^{4}$ | $-3^{5}$ / $9^{0}$ | $-4^{3}$ / $4^{5}$ | $00$ / $00$ | $+4^{0}$ / $10$ | $+4^{8}$ / $14^{8}$ | | |
| $56^{9}$ | ✓ | $-4^{0}$ / $15^{0}$ | $-3^{2}$ / $9^{0}$ | $00$ / $3^{5}$ | $+2^{4}$ / $00$ | $+5^{0}$ / $10$ | $+5^{8}$ / $15^{8}$ | $+13^{4}$ / $60$ | |
| | ✓ | $-0^{7}$ / $10^{0}$ | $-0^{5}$ / $9^{0}$ | $00$ / $7^{0}$ | $00$ / $00$ | $00$ / $10$ | | | |
| $32^{3}$ | ✓ | $-2^{6}$ / $12^{9}$ | $-1^{9}$ / $9^{0}$ | $00$ / $00$ | $+2^{9}$ / $8^{6}$ | $+5^{3}$ / $10$ | $+5^{3}$ / $15^{3}$ | $+13^{2}$ / $55$ | |

| Station | Elev. | Grade. | | | | |
|---|---|---|---|---|---|---|
| 1335+50 | 21.2 | 19.0 | | | 21.1 | 10 |
| 1335+60 | 26.3 | | | | 19.6 | 13 |
| +73.0 | 19.0 | | | | 26.2 | 5 |
| 1336 | 17.6 | | | | 35.7 | 7 |
| | 1-1X1=24 | 1-1X1=12 | | | | |
| +25 | 19.0 | | | | 20.3 | 2 |
| 1336+50 | 20.8 | | | | 18.0 | 65 |
| +86.5 C.C. | | Level | | | 44.0 | 18 |
| | | | | | X | 3 |
| +46.5 | 15.5 | | | | | |
| +76.5 | 14.3 | | | | 84.9 | |
| +94.6 | 19.0 | | | | 59.1 | 5 |
| 1338+06.5 E.C. | 20.9 | | | | 47.7 | 7 |
| 1338+16.0 | 19.0 | | | | 50.4 | 1 |
| +50 | 12.0 | | | | 182.2 | |
| +90 | 13.4 | 19.00 | | | 212.5 | |

| | | ₵ |
|---|---|---|
| 1 | $107^{7}$ | $-3^{7}$ / $14^{5}$ $-3^{5}$ / $9^{0}$ $00$ / $2^{6}$ $+2^{2}$ / $00$ $+8^{2}$ / $10$ $+11$ / $21$ $\left(+12^{8}\right.$ / $30$ $+16^{6}$ / $60\left.\right)$ |
| 6 | $139^{5}$ | $-3^{8}$ / $14^{7}$ $-3^{2}$ / $9^{0}$ $00$ / $3^{0}$ $+7^{3}$ / $00$ $+8^{5}$ / $10$ $+11^{2}$ / $21^{2}$ |
| 2 | $50^{0}$ | $-3^{8}$ / $14^{7}$ $-3^{5}$ / $9^{0}$ $00$ / $00$ $+5^{5}$ / $10$ $+10^{0}$ / $20$ |
| 7 | $7^{0}$ | $-3^{2}$ / $13^{8}$ $-3^{2}$ / $9^{0}$ $-2^{8}$ / $2^{0}$ $-1^{4}$ / $00$ $00$ / $4^{0}$ $+1^{6}$ / $10$ $+2^{3}$ / $12^{3}$ $+13^{0}$ / $50$ |
| 3 | $28^{3}$ | $-3^{0}$ / $13^{5}$ $-3^{0}$ / $9^{0}$ $00$ / $00$ $+3^{8}$ / $10$ $+4^{5}$ / $14^{5}$ |
| 8 | $65^{4}$ | $-3^{0}$ / $14^{5}$ $-3^{0}$ / $9^{0}$ $-3^{0}$ / $7^{0}$ $00$ / $3^{6}$ $+1^{8}$ / $00$ $+6^{6}$ / $10$ $+11^{3}$ / $21^{3}$ $+18^{8}$ / $55$ |
| 24 | $181^{3}$ | $-4^{4}$ / $15^{6}$ $-4^{7}$ / $9^{0}$ $-4^{9}$ / $5^{0}$ $00$ / $1^{0}$ $+0^{6}$ / $00$ $+1^{4}$ / $3^{0}$ $+7^{6}$ / $10$ $+13^{4}$ / $20$ $+15^{7}$ / $25^{7}$ $\left(+16^{8}\right.$ / $30$ $+22^{8}$ / $50$ |
| | $36^{4}$ | $-11^{1}$ / $25^{6}$ $-11^{1}$ / $20$ $-5^{6}$ / $12^{5}$ $-5^{2}$ / $9^{0}$ $-5^{4}$ / $1^{5}$ $-3^{5}$ / $00$ $00$ / $7^{1}$ $+2^{6}$ / $10$ $+10^{2}$ / $20^{2}$ $\left(+24^{2}\right.$ / $42$ $+28^{7}$ / $55\left.\right)$ |
| 49 | $29^{3}$ | $-9^{4}$ / $19^{4}$ $5^{0}$ / $9^{0}$ $-3^{7}$ / $00$ $00$ / $4^{5}$ $+3^{0}$ / $10$ $+7^{7}$ / $17^{7}$ |
| 9 | $53^{7}$ | $-6^{0}$ / $18$ $-6^{0}$ / $9$ $-6^{8}$ / $8^{5}$ $00$ / $00$ $+2^{4}$ / $2^{0}$ $+9^{4}$ / $19^{4}$ |
| 2 | $71^{2}$ | $-5^{6}$ / $17^{4}$ $-6^{0}$ / $9^{0}$ $00$ / $2^{1}$ $+1^{9}$ / $00$ $+5^{6}$ / $10$ $+8^{8}$ / $18^{8}$ $+21^{5}$ / $55$ |
| 0 | $18^{2}$ | $-6^{4}$ / $18^{6}$ $-6^{1}$ / $9^{0}$ $-0^{8}$ / $3^{5}$ $00$ / $00$ $+2^{7}$ / $10$ $+3^{2}$ / $13^{2}$ |
| 82 | | $-10^{1}$ / $24^{1}$ $-6^{8}$ / $9^{0}$ $-7^{0}$ / $00$ $-3^{8}$ / $9^{0}$ $-3^{0}$ / $13^{5}$ $00$ / $29$ $+7^{0}$ / $55$ |
| 12 | | $-11^{3}$ / $25^{9}$ $-7^{8}$ / $9^{0}$ $-5^{6}$ / $00$ $-5^{9}$ / $9^{0}$ $-4^{9}$ / $16^{3}$ $00$ / $37$ $+4^{3}$ / $55$ $+6^{6}$ / $60$ |

| Station | Elev. | Grade | Cut. | Fill. | |
|---|---|---|---|---|---|
| 1339+60 | $12^{6}$ | $19^{0}$ | | | $241^{2}$ |
| | 1-Box 1'x2'-36' (-24 ft of 1x1-) | | | | |
| 1340 | $12^{6}$ | | | | 250. |
| +50 | $12^{8}$ | | | | |
| 1341 | $13^{3}$ | | | | |
| +50 | $14^{3}$ | Level. | | | $164^{7}$ |
| 1342 | $14^{7}$ | | | | |
| +50 | $14^{7}$ | | | | |
| 1343 | $14^{7}$. | | | | |
| +50 | $15^{5}$ | X $19^{00}$ | | | |
| 1344 | $11^{9}$ | $18^{6875}$ | | | |
| +50 | $11^{9}$ | $18^{375}$. | | | |
| | 1-1x1=36' | =1-1'x1'-18' | | | |
| +90 | $11^{1}$ | $18^{07}$ | | | |
| 1345+50 | $11^{2}$ | $17^{75}$ | | | $159^{6}$ |
| 1346+10 | $12^{3}$ | $17^{3869}$ | | | $134^{6}$ |
| | 1-1x1 Box 30 | | | | |

LEFT. ℄ RIGHT.

$\frac{-11^{0}}{25^{5}}$ $\frac{-9^{2}}{9^{0}}$ $\frac{-6^{4}}{00}$ $\frac{-6^{1}}{9^{0}}$ $\frac{-6^{6}}{18^{8}}$

$\frac{-12^{0}}{27^{0}}$ $\frac{-8^{7}}{9^{0}}$ $\frac{-6^{4}}{00}$ $\frac{-6^{4}}{9^{0}}$ $\frac{-6^{5}}{18^{7}}$ | $\frac{-4^{5}}{12^{0}}$ $\frac{-2^{5}}{6^{0}}$ $\frac{00}{\text{℄}}$ (40) $\frac{+3^{1}}{6^{0}}$ $\frac{+9^{0}}{15}$ (5.5)

$\frac{-11^{9}}{26^{8}}$ $\frac{-9^{0}}{10^{5}}$ $\frac{-7^{8}}{9^{0}}$ $\frac{-6^{2}}{00}$ $\frac{-5^{9}}{9^{0}}$ $\frac{-3^{0}}{14^{5}}$ $\frac{00}{21^{8}}$ $\frac{+16^{5}}{55}$

Rock.

$\frac{-11^{4}}{26^{1}}$ $\frac{-9^{5}}{12^{5}}$ $\frac{-6^{9}}{9^{0}}$ $\frac{-5^{7}}{00}$ $\frac{-5^{1}}{6^{0}}$ $\frac{00}{10^{0}}$ $\frac{+11}{25}$ $\frac{+22^{6}}{35}$ $\frac{+27^{7}}{55}$

(M) Water

$\frac{-22^{9}}{34^{3}}$ $\frac{-17^{2}}{22}$ $\frac{-11^{2}}{20}$ $\frac{-7^{8}}{12}$ $\frac{-5^{0}}{9^{0}}$ $\frac{-4^{7}}{00}$ $\frac{-4^{8}}{6^{0}}$ $\frac{-1^{7}}{9^{0}}$ $\frac{-1^{1}}{10^{6}}$ $\frac{00}{12^{2}}$ $\frac{+21^{2}}{55}$

$18^{9}$ Water $\frac{-21^{9}}{32^{8}}$ $\frac{16^{5}}{26}$ $\frac{-9^{3}}{21^{0}}$ $\frac{-4^{6}}{9^{0}}$ $\frac{-4^{3}}{00}$ $\frac{00}{4^{7}}$ $\frac{+4^{3}}{10}$ $\frac{+6^{8}}{16^{8}}$ $\frac{+27^{0}}{55}$

Water. $\frac{-22^{2}}{33^{4}}$ $\frac{-17^{4}}{28}$ $\frac{-13^{6}}{15^{3}}$ $\frac{-4^{1}}{6^{0}}$ $\frac{-4^{3}}{00}$ $\frac{-4^{6}}{5^{0}}$ $\frac{00}{10^{0}}$ $\frac{+3^{0}}{15}$ $\frac{+21^{7}}{55}$

Water. $\frac{-20^{6}}{27^{0}}$ $\frac{-15}{16^{0}}$ $\frac{-9^{0}}{9^{0}}$ $\frac{-4^{7}}{4^{0}}$ $\frac{-4^{3}}{00}$ $\frac{-4^{0}}{9^{0}}$ $\frac{+2^{2}}{12^{3}}$ $\frac{00}{16^{5}}$ $\frac{+7^{1}}{28}$ $\frac{+14^{6}}{48}$

$\frac{-20^{1}}{34}$ $\frac{-13^{5}}{20}$ $\frac{-7^{5}}{10^{5}}$ $\frac{-4^{0}}{9^{0}}$ $\frac{-3^{2}}{7^{0}}$ $\frac{-3^{5}}{00}$ $\frac{-4^{0}}{9^{0}}$ $\frac{00}{12^{0}}$ $\frac{+9^{3}}{30}$ $\frac{+21^{0}}{47^{0}}$ $\frac{+28^{8}}{59^{0}}$

$\frac{-21^{0}}{31}$ $\frac{-11^{2}}{10^{0}}$ $\frac{-7^{9}}{8^{0}}$ $\frac{-6^{8}}{00}$ $\frac{-5^{1}}{9^{0}}$ $\frac{-4^{1}}{15^{2}}$ $\frac{-3^{6}}{25}$ $\frac{00}{30^{5}}$ $\frac{+15^{5}}{55}$

$\frac{-19^{2}}{36}$ $\frac{-7^{8}}{18}$ $\frac{-7^{2}}{9^{0}}$ $\frac{-6^{5}}{00}$ $\frac{-5^{6}}{9^{0}}$ $\frac{-4^{0}}{15}$

$\frac{-18^{5}}{36^{7}}$ $\frac{-8^{3}}{20}$ $\frac{-8^{0}}{9^{0}}$ $\frac{-7^{0}}{00}$ $\frac{-5^{8}}{9^{0}}$ $\frac{-3^{9}}{13^{7}}$

$\frac{-8^{0}}{21^{0}}$ $\frac{-7^{0}}{9^{0}}$ $\frac{-6^{4}}{00}$ $\frac{-4^{3}}{9^{0}}$ $\frac{-2^{5}}{12^{6}}$

$\frac{-7^{3}}{19^{9}}$ $\frac{-6^{6}}{9^{0}}$ $\frac{-5^{1}}{00}$ $\frac{-3^{9}}{9^{0}}$ $\frac{-3^{1}}{13^{6}}$

| | Elev | Grade. | Cut | Fill. |
|---|---|---|---|---|
| 1346+50 | $-8^{8}$ | $17^{125}$ | | |
| | | 14 / 3.1 | | |
| 1347 | $9^{8}$ | $16^{8125}$ | | |
| +50 | $9^{7}$ | $16^{5}$ | | |
| 1348 | $10^{5}$ | $16^{1875}$ | | |
| +50 | $12^{0}$ | $15^{875}$ | | |
| 1349 | $13^{9}$ | $15^{5625}$ | | |
| +50 | $13^{5}$ | $15^{250}$ | | |
| 1350 | $13^{3}$ | $14^{9375}$ | 2.2 | |
| | | 3125 | | |
| +50 | $13^{3}$ | 14.625 | | |
| 1351 | $13^{3}$ | 14.3125 | | |
| +50 | | ✓14.0 | | |

−0625

73
5
15.5
23.0

Lt C Rt

| Area | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| $210^{0}$ | | $-8^{9}/22^{3}$ | $-8^{7}/9^{0}$ | $-8^{3}/00$ | $-5^{7}/9^{0}$ | $-3^{5}/14^{2}$ | | | | |
| $15^{2}$ | | $-6^{7}/19^{0}$ | $-6^{7}/9^{0}$ | $-7^{0}/06$ | $-3^{9}/9^{0}$ | $-3^{0}/13^{5}$ | $-3^{0}/16$ | | | |
| $162^{0}$ | | $-6^{6}/18^{9}$ | $-6^{8}/9^{0}$ | $-6^{8}/00$ | $-5^{0}/9^{0}$ | $-4^{2}/15^{3}$ | $-3^{4}/22$ | $00/26$ | $+4^{0}/29$ | $+6^{8}/36$ | $+12/41$ |
| $124^{6}$ | | $-5^{1}/16^{6}$ | $-5^{7}/9^{0}$ | $-5^{7}/00$ | $-4^{2}/9^{0}$ | $-3^{8}/14^{7}$ | $-4^{0}/23$ | $00/26^{5}$ | $+12^{0}/40$ | $+24/55$ |
| $81^{0}$ | | $-3^{2}/13^{8}$ | $-3^{5}/9^{0}$ | $-3^{9}/00$ | $-3^{2}/9^{0}$ | $-3^{2}/13^{8}$ | $00/21$ | $+5^{5}/26^{0}$ | $+11^{5}/38$ | |
| $46^{0}$ | | $-4^{5}/15^{7}$ | $-2^{2}/9^{0}$ | $-1^{7}/00$ | $-2^{0}/9^{0}$ | $-2^{4}/12^{6}$ | $00/17^{7}$ | $+1^{3}/20$ | $+8^{0}/40$ | |
| $23^{0}$ | 00 | $-2^{0}/12^{0}$ | $-2^{0}/9^{0}$ | $-1^{7}/00$ | $00/4^{0}$ | $00/10$ | $00/20$ | $+5^{0}/37$ | $+8^{5}/50$ | |
| $20^{7}$ | $1^{7}$ | $-1^{5}/17^{2}$ | $-1^{5}/9^{0}$ | $-1^{6}/00$ | $00/7^{0}$ | $+0^{7}/10$ | $+0^{8}/10^{8}$ | $+0^{5}/25$ | $+5^{9}/36$ | $+13^{3}/58$ |
| $20^{1}$ | 00 | $-1^{2}/10^{8}$ | $-1^{2}/9^{0}$ | $-1^{3}/00$ | $-0^{4}/9^{0}$ | $-0^{4}/9^{6}$ | | | | |
| $17^{7}$ | | $-0^{7}/10$ | $-0^{7}/9^{0}$ | $-1^{0}/00$ | $-0^{6}/9^{0}$ | $-0^{5}/9^{7}$ | | | | |

# County Road

| | | |
|---|---|---|
| 1350 | | ℄ 22° ft Rt. |
| 1349+50 | | ℄ 21° ft Rt |
| 1349 | | ℄ 22° ft R. |
| 1348+50 | | ℄ 21° ft R. |
| 1348 | | ℄ 22 ft R. |
| 1347+50 | | ℄ 21 ft R. |
| | | |
| | | |
| | | |
| 1344 | Gr-4 | ℄ 22° ft R. |
| 1343+50 | G-3 | ℄ 23° R. |
| 1343 | G-2 | ℄ 22° R. |
| 1342+50 | G-1 | ℄ 22° R |
| 1342 | | ℄ 22° R |
| 1341+50 | | ℄ 22° R |

16
6
22

7.9
6.5
16.4
5.3
11.1

11.8
5.3
6.5
9.6

23.7
33
7
26 - 20.7

$\frac{00}{6^0}$ $\frac{00}{00}$ $\frac{00}{3}$ $\frac{+1^8}{6^0}$ $\frac{+4^8}{10^8}$

$\frac{00}{6^0}$ $\frac{00}{00}$ $\frac{+2^0}{6^0}$ $\frac{+2^9}{8^9}$

$\frac{+1^6}{6^0}$ $\frac{+4^2}{00}$ $\frac{+6^3}{6^0}$ $\frac{+9^3}{15^3}$

$\frac{00}{6^0}$ $\frac{+3^0}{00}$ $\frac{+8^0}{6^0}$ $\frac{+18^3}{24^3}$

$\frac{00}{6^0}$ $\frac{00}{00}$ $\frac{00}{2^0}$ $\frac{+4^5}{6^0}$ $\frac{+27^0}{33^0}$

$\frac{00}{6^0}$ $\frac{+0^5}{00}$ $\frac{+5^0}{6^0}$ $\frac{+15^5}{21^5}$

$\frac{00}{6^0}$ $\frac{00}{00}$ $\frac{00}{3}$ $\frac{+2^3}{6^0}$ $\frac{-7^5}{13^5}$

$\frac{+5^3}{6^0}$ $\frac{+8^5}{00}$ $\frac{+11^1}{6^0}$ $\frac{+34^2}{32^0}$

$\frac{+2^0}{6^0}$ $\frac{+6^5}{00}$ $\frac{+9^6}{6^0}$ $\frac{16^1}{26^0}$

$\frac{+4^4}{6^0}$ $\frac{+7^0}{00}$ $\frac{+9^6}{6^0}$ $\frac{+20^7}{26^7}$

16
4.7
11.3

$\frac{00}{11^3}$ $\frac{+6^8}{6^0}$ $\frac{+10^3}{00}$ $\frac{+14^0}{6^0}$ $\frac{+27^0}{33}$

$\frac{+2^0}{6^0}$ $\frac{+3^8}{00}$ $\frac{+7^5}{6^0}$ $\frac{+14^4}{20^4}$

| | | | | |
|---|---|---|---|---|
| 1341 | | ℄ 21° R- | | |
| 1340+50 | | ℄ 22° R- | | |
| 1340 | | ℄ 22° R | | |
| 1339+60 | | ℄ 22° R | | |
| 1338+90 | | ℄ 22 R | | |
| 1338+50 | | ℄ 22 R | | |
| 1338+05 | G- +2° | ℄ 21° R | | |
| +71 | | | | |
| 1337+46 | G +3° | ℄ 21° R | | |
| 1336+86 | G +3° | ℄ 24° | | |
| 1336+50 | G+3 | ℄ 24° | | |
| 1336 | G+3 | ℄ 22 | | |
| 1335+50 | G+3 | ℄ 24 | | |
| 1335 | G+32 | ℄ 24 | | |

$\frac{+3^{0}}{6^{0}}$ $\frac{+8^{0}}{00}$ $\frac{+14}{6^{0}}$ $\frac{+27^{7}}{33}$

$\frac{-2^{4}}{6^{0}}$ $\frac{00}{00}$ $\frac{+3^{0}}{6}$ $\frac{+6^{0}}{12}$

$\frac{00}{13}$ $\frac{-4^{8}}{6^{0}}$ $\frac{-5^{6}}{00}$ $\frac{-3^{0}}{6^{0}}$ $\frac{00}{18^{0}}$

$\frac{}{00}$

$\frac{00}{13}$ $\frac{-4^{5}}{6^{0}}$ $\frac{-3^{5}}{00}$ $\frac{-2^{0}}{6^{0}}$ $\frac{00}{15^{0}}$

$\frac{00}{13}$ $\frac{-2^{6}}{6^{0}}$ $\frac{-1^{4}}{00}$ $\frac{00}{6^{8}}$

$\frac{00}{9^{0}}$ $\frac{+3^{0}}{6^{0}}$ $\frac{+7^{5}}{00}$ $\frac{+9^{7}}{6^{0}}$ $\frac{+15^{0}}{21^{0}}$

$\frac{00}{9^{0}}$ $\frac{-2^{0}}{6^{0}}$ $\frac{+8^{5}}{00}$ $\frac{+12^{0}}{6^{0}}$ $\frac{+24^{9}}{29^{9}}$

$\frac{00}{8^{0}}$ $\frac{+2^{0}}{6^{0}}$ $\frac{+7^{8}}{00}$ $\frac{+11^{5}}{6^{0}}$ $\frac{+24^{0}}{29^{9}}$

$\frac{00}{11^{0}}$ $\frac{+9^{2}}{6^{0}}$ $\frac{+11^{9}}{00}$ $\frac{+13^{7}}{6^{0}}$ $\frac{+19^{6}}{25^{6}}$

$\frac{00}{11}$ $\frac{+6^{9}}{6^{0}}$ $\frac{+8^{9}}{00}$ $\frac{+10^{3}}{6^{0}}$ $\frac{+12^{9}}{18^{9}}$

$\frac{00}{6^{0}}$ $\frac{+1^{9}}{00}$ $\frac{+3^{6}}{6^{0}}$ $\frac{+6^{0}}{12^{0}}$

$\frac{00}{11^{0}}$ $\frac{+7^{2}}{6^{0}}$ $\frac{+8^{5}}{00}$ $\frac{+9^{8}}{6^{0}}$ $\frac{+11^{2}}{17^{2}}$

$\frac{00}{11}$ $\frac{+2^{9}}{6^{0}}$ $\frac{+3^{9}}{00}$ $\frac{+5^{0}}{6^{0}}$ $\frac{+6^{3}}{12^{3}}$

# County Road

| | | | | |
|---|---|---|---|---|
| 1334+50 | G+3° | ℄ 22 R | | |
| 1334+09 | G+2 | ℄ 22 R. | | |
| 1334+13 | | ℄ 22 R. | | |
| 1333+80 | | ℄ 20° Rt. | | |
| 1333+50 | | ℄ 24° Rt | | |
| 1333+20 | | ℄ 20° Rt | 20 15 5 | |
| 1332+93 | G+2° | ℄ 24 | | |
| 1332+50 | G+1° | ℄ 21 | | |
| 1332 | G+1° | ℄ 21 | 22 15 7 20 0 22 4 | |
| 1331+50 | G+1° | ℄ 22 | | |
| 1331 | G+1° | ℄ 22 | | |
| 1330+50 | G+1° | ℄ 22 | | |
| 1330+00 | G+3° | ℄ 23 | | |
| 1329+50 | G+2° | ℄ 27 | | |
| 1329+00 | G+1 | ℄ 33 | | |
| 1328+42.77 | G+1° | ℄ 25 Rt. | | |

May 21-1913 37

41
15
26

| | | | |
|---|---|---|---|
| 00 / 9 | +2 8 / 6 | +3 8 / 00 | +4 9 / 6 |
| +6 / 12 | | | |
| 00 / 10 | +3 1 / 6 | +4 1 / 00 | +5 1 / 6 |
| +6 / 12 | | | |
| 00 / 12 | +1 5 / 6 | +2 3 / 00 | +3 2 / 6 |
| +4 2 / 12 | | | |
| −3 5 / 6 | −1 2 / 00 | 00 / 6 | |
| −4 7 / 6 | −2 2 / 00 | 00 / 6 | |
| 00 / 6 | 00 / 4 | +2 / 00 | +4 2 / 6 |
| +6 3 / 12 | | | |
| 00 / 9 | +1 2 / 6 | +3 2 / 00 | +5 3 / 6 |
| +8 / 14 | | | |
| 00 / 7 | +2 3 / 6 | +4 1 / 00 | +5 8 / 6 |
| +7 8 / 13 | | | |
| 00 / 7 | +3 8 / 1 | +5 6 / 00 | +7 2 / 6 |
| +9 8 / 15 | | | |
| 00 / 7 | +6 3 / 6 | +8 8 / 00 | +11 4 / 6 |
| +19 / 25 | | | |
| 00 / 8 | +6 1 / 6 | +9 1 / 00 | +12 3 / 6 |
| +19 4 / 25 | | | |
| 00 / 8 | +2 / 6 | +5 8 / 00 | +1 4 / 6 |
| +7 3 / 13 | | | |
| 00 / 6 | +3 7 / 00 | +5 8 / 6 | +8 5 / 14 |
| 00 / 6 | +1 8 / 00 | +3 5 / 6 | +5 / 11 |
| 00 / 8 | +1 2 / 00 | +2 / 6 | +2 / 8 |
| 00 / 7 | +0 7 / 00 | +1 2 / 6 | +1 3 / 7 |

Spur for Layton Lumber Co.
at Markham

+50

17

+50

16

+50

15

+50

14 {center Road} 50 ft Wide

+50

13

+50

12

+50

11

+50

10

9+56.5 P.O.T

from Page 26

| | | | | |
|---|---|---|---|---|
| +50 | | | | |
| +07.30 | E.C. | 19° 13½' | | |
| 28 | | 18° 42½' | | |
| +50 | | 15° 12½' | | |
| 27 | | 11° 42½' | △ 38°27' | (3) |
| +50 △ | | 8° 12½' | St. 142.49 | |
| 26 | | 4° 42½' | | |
| +50 | | 1° 12½' | | |
| +32.66 | B.C. 14° Rt. | 0°00 | | |
| 25 | | | | |
| +50 | | | | |
| 24 | | | | |
| +99.39 | E.C. | 13°06' | | |
| +50 | | 9°38' | △ 26°12' | (2) |
| 23 | | 6°08' | St 95.30 | |
| +50 | | 2°38' | | |
| +12.25 | B.C. 14° Lt. | 0°00 | | |
| 22 | | | | |
| +50 | | | | |
| 21 | | | | |
| +50 △ P.O.T. | | | | |
| +44.06 | E.C. | 10°30' ✓ | | |
| 20 | | 7°25' ✓ | △ 21° | |
| +50 | | 3°55' ✓ | St. 75.9 | (1) |
| 19 | | 0°25' | | |
| 18 +94.06 | B.C. 14° Rt. | 0°00 | | |
| +50 | | | | |
| 18 | | | | |

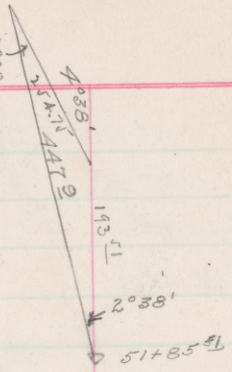
700
300
1°45'

# Spur for Laton Lumber Co.

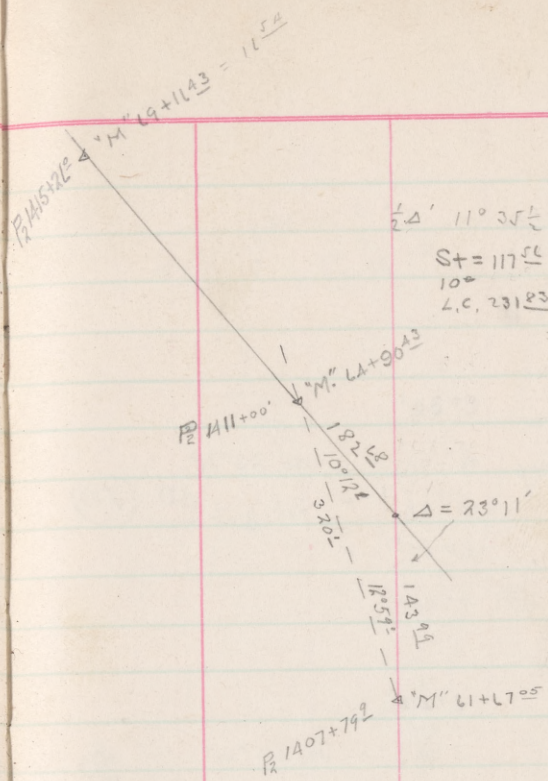
| | | | | | |
|---|---|---|---|---|---|
| 41 | +83.25 | E.C. △ | 14°10½' ✓ | | |
| | +50 | | 11°51' ✓ | | |
| 41 | △ | | 8°21' ✓ | △ 28°21' | (4) |
| | +50 | | 4°51' ✓ | St. 103.43 | |
| 40 | | | 1°21' ✓ | | |
| | +80.75 | B.C. 14°L. △ | 0°00' ✓ | | |
| | +50 | | | | |
| 39 | | | | | |
| | +50 | | | | |
| 38 | | | | | |
| | +50 | | | | |
| 37 | | | | | |
| | +50 | | | | |
| 36 | | | | | |
| | +50 | | | | |
| 35 | | | | | |
| | +50 | | | | |
| 34 | | △ | | | |
| | +50 | | | | |
| | +39 | Top Bank | | | |
| 33 | | Top Bank | | | |
| | +60 | | | | |
| | +50 | on tree | | | |
| 32 | | | | | |
| | +73.57 | △ | | | |
| | +50 | | | | |
| 31 | | | | | |
| | +50 | | | | |
| 30 | | | | | |
| | +50 | | | | |
| 29 | | | | | |

# Spur for Laton Lumber Co

| | | | | |
|---|---|---|---|---|
| +50 | | | | |
| 52 | | | | |
| 5+85 51 | P.O.T. | | | |
| +50 | | | | |
| 51 | | | | |
| +50 | | | | |
| 50 | | | | |
| 4+94 67 | P.O.T. | | | |
| +58 | | | | |
| 49 | | | | |
| +50 | | (End Trench 8/7/51) | | |
| +41 31 | P.O.T. | | | |
| +17 36 | P.O.T. | | | |
| 48 | | | | |
| +50 | | | | |
| 47 | | | | |
| +50 | | | | |
| 46 | | | | |
| +23° | E.C. | Δ 8°25' | | |
| +03 84 | | Δ 7°27½' | | |
| 45 | | 7°16' | Δ ~~14°55'~~ | Δ 16°50' |
| +50 | | 4°41' | ~~St. 75 03~~ | |
| 44 | | 7°16' | St 84 80 | (5) |
| +54 47 | B.C. 10° | R+. 40°00' | | |
| +50 | | | | |
| 43 | | | | |
| +50 | | | | |
| 42 | | | | |


2°00'
4°38'
447.9
193.51
2°38'
51+85.51

| | | | | |
|---|---|---|---|---|
| 63 | | 5° 19½ | | |
| +50 | | 2° 49½ | Δ 23°11' | (8) |
| 62 | | 0° 19½ | St. 117 56 | |
| 61+93 48 | B.C. 10+ Lt. | 0°00' | | |
| 61+67 05 | P.O.T. | | | |
| +50 | | | | |
| 61 | | | | |
| +88 5 | E.C. 14° | 13°55' | | |
| +50 | | 11°14' 2°41' | | |
| 60 | | 7°44' 3°30' | Δ 27°50' | (7) |
| +50 | | 4°14' 3°41' | St. 101 47 | |
| 59 | | 0°44' | | |
| +89 7 | B.C. 14+ Rt. | 0+00 | | |
| +50 | | | | |
| 58 | | | | |
| +50 | | | | |
| 57 | | | | |
| +50 | | | | |
| +33 7 | P.O.T. | | | |
| 56 | | | | |
| +50 | | | | |
| 55 | | | | |
| +50 | | | | |
| +36 9 | E.C. | 2°19' | | |
| 54 | | 1°34' | Δ = 4°38 | (6) |
| +50 | | 0°34' | St. - 57 95 | |
| +21 07 | B.C. 4° Lt. | 0°00 | | |
| 53 | | | | |




$\frac{1}{2}\Delta'$ 11° 35½ = 9.312006
2.758260
2.070266 =
038 = 117.56
228

St = 117.56
10°
L.C. 231.83

2.158330 = 143.99
9.248181 = Log 10°12
0.404813
2.505286
9.351540 Log. 12°59
2.261689 = 182.68

+50

73

+50

+48

72

71 +99 74 E.C. 2°48 11°39'

+59 74

+50 8°11 Δ 23°18

+38 74 4°16

71 4°41 ✓ St. 8 11 43 (10)

+50 10°11' ✓

+33 1/2 B.C 11° Rt. 0°00' ✓

70

69 +64 20 E.C. 6°42½ ✓

+50 5°43 ✓ Δ 13°25

69 2°12' ✓ St. 48 17 (9)

68 +68 37 B.C, 14° Lt 0°00 ✓

+50

68

+50

67

+50

66

+50

65

64 +90 43 P.O.T

+50

64 +25 31 E.C. Δ 11°35½' ✓

64 10°19½ ✓

63 +50 7°49½

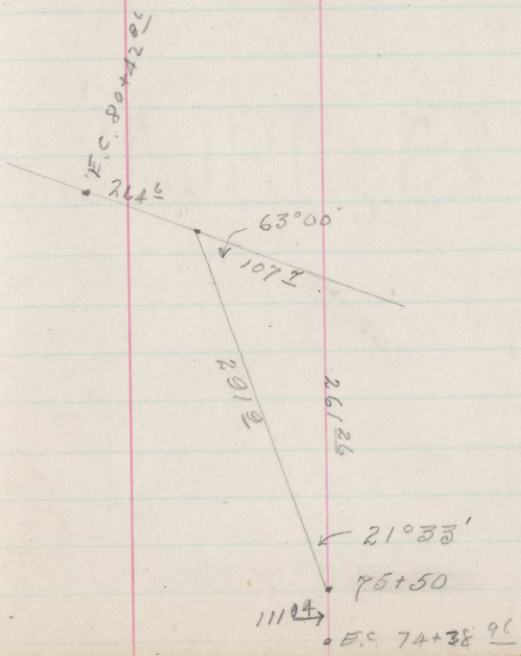
166.64 70+30.5
14 / 23.3

St 84°43'
14° Rt.

80
18
62
24
38

40
14
24

| | | | | |
|---|---|---|---|---|
| 83 △ | End. | | | |
| +50 | | | | |
| 82 | | | | |
| +50 | | | | |
| 81 | | | | |
| +50 | | | | |
| +42 86 △ | EC 14° | 42° 16½ | 0° 00 | ✓ |
| 80 | | 39° 16½ | 3° 00 | ✓ |
| +50 | | 35° 46½ | 6° 30 | ✓ |
| 79 | | 32° 16½ | 10° 00 | ✓ △ |
| +50 | | 28° 46½ | 13° 30 | ✓ |
| 78 △ | | 25° 16½ | 17° 00 | ✓ |
| +50 | | 21° 46½ | 19° 00' − 30 / 20° 00 − 30 | |
| 77 | | 18° 16½ | 24° 00' △ (11) | |
| +50 | | 14° 46½ | 27° 30 | |
| 76 | | 11° 16½ | 31° 00 | |
| +50 △ | | 7° 46½ | 34° 30' | |
| 75 | | 4° 16½ | 38° 00 ✓ | △ 84°33' St 37°31 |
| +50 | | 0° 46½ | 41° 30 ✓ | |
| +38 96 ▽ | BC 14° | 0° 00 | 42° 16½ ✓ | |
| 74 | | | | |


E.C. 80+42 96
264 6
63°00'
107 7
291 9
261 26
21°33'
75+50
111 04
E.C. 74+38 96

| | + | π | − | Rod. |
|---|---|---|---|---|
| B.M. | $4^{35}$ | $18^{606}$ | | |
| 1350+85 c.c. | | | | $5^{3}$ |
| 1351 | | | | $5^{2}$ |
| +50 | | | | $4^{8}$ |
| 1352 | | | | $4^{2}$ |
| +50 | | | | $5^{3}$ |
| 1353 | | | | $5^{4}$ |
| +50 | | | | $5^{3}$ |
| 1354 | | | | $5^{3}$ |
| +24 53 | | | | $5^{2}$ |
| T.P. | $6^{427}$ | $19^{962}$ | $5^{071}$ | |
| +54 53 | | | | $6^{4}$ |
| +84 53 | | | | $6^{1}$ |
| 1355+14 53 | | | | $5^{8}$ |
| 1355+44 53 | E.C 10° | | | $5^{7}$ |
| M 9+56 56 | P.O.T. | | | |
| 10 | | | | $5^{2}$ |
| +50 | | | | $4^{7}$ |
| 11 | | | | $4^{3}$ |
| +50 | | | | $3^{9}$ |
| 12 | | | | $3^{5}$ |
| +50 | | | | $3^{1}$ |
| 13 | | | | $2^{9}$ |
| +50 | | | | $2^{4}$ |
| T.P. | $10^{508}$ | $28^{235}$ | $2^{235}$ | |
| 14 | | | | $10^{2}$ |
| +50 | | | | $10^{2}$ |
| 15 | | | | $10^{1}$ |

| | | | |
|---|---|---|---|
| $14^{\underline{256}}$ | B.M. on R.W. tree Lt 1350+25 | | |
| | Elev. $14^{\underline{256}}$ | | |
| $13^{\underline{3}}$ | | | |
| $13^{\underline{4}}$ | | | |
| $13^{\underline{8}}$ | | | |
| $13^{\underline{7}}$ | | | |
| $13^{\underline{3}}$ | | | |
| $13^{\underline{2}}$ | | | |
| $13^{\underline{3}}$ | | | |
| $13^{\underline{3}}$ | | | |
| $13^{\underline{4}}$ | | | |
| $13^{\underline{535}}$ | T.P. | | |
| $13^{\underline{5}}$ | | | |
| $13^{\underline{8}}$ | | | |
| $14^{\underline{1}}$ | | | |
| $14^{\underline{2}}$ | | | |
| $14^{\underline{7}}$ | | | |
| $15^{\underline{2}}$ | | | |
| $15^{\underline{6}}$ | | | |
| $16^{\underline{0}}$ | | | |
| $16^{\underline{4}}$ | | | |
| $16^{\underline{8}}$ | | | |
| $17^{\underline{0}}$ | | | |
| $17^{\underline{5}}$ | | | |
| $17^{\underline{727}}$ | T.P. | | |
| 18 | | | |
| 18 | | | |
| $18^{\underline{1}}$ | | | |

| | + | × | − | Rod |
|---|---|---|---|---|
| +50 | | 28 235 | | 9 6 |
| 16 | | | | 8 9 |
| +50 | | | | 8 4 |
| 17 | | | | 7 3 |
| +50 | | | | 6 2 |
| 18 | | | | 4 7 |
| +50 | | | | 3 6 |
| B.M. | | 28 235 | | 1 311 |
| +94 06 | B.C 14° | | | 2 8 |
| 19 | | | | 2 5 |
| T.P. | 6 185 | 32 601 | 1 891 | |
| +50 | | | | 5 7 |
| 20 | | | | 6 1 |
| +50 | | | | 6 3 |
| 21 | | | | 5 8 |
| +19 2 | Top bank. | | | 6 9 |
| +24 } | Bot. Creek. | | | 11 5 |
| +42 } | | | | 10 9 |
| +65 | Top bank. | | | 5 5 |
| 22 | | | | 5 2 |
| +12 25 | E.C. | | | 4 8 |
| +50 | | | | 4 7 |
| 23 | | | | 3 5 |
| +50 | | | | 1 6 |
| T.P. | 5 304 | 36 958 | 0 947 | |
| 24 | | | | 7 3 |
| +50 | | | | 6 2 |
| 25 | | | | 5 8 |

| Elev. | | | |
|---|---|---|---|
| 18 6 | | | |
| 19 3 | | | |
| 19 8 | | | |
| 20 9 | | | |
| 22 0 | | | |
| 23 5 | | | |
| 24 6 | | | |
| 26 924 | B.M. on Rdw stump 14ft Lt | | |
| 25 4 | Eng. Sta. M. 18+86 Elev. 26 924 | | |
| 25 7 | | | |
| 26 416 | T.P. | | |
| 26 9 | | | |
| 26 5 | | | |
| 26 3 | | | |
| 26 8 | | | |
| 25 7 | | | |
| 21 1 | | | |
| 21 7 | | | |
| 27 1 | | | |
| 27 4 | | | |
| 27 8 | | | |
| 27 9 | | | |
| 29 1 | | | |
| 30 0 | | | |
| 31 654 | T.P. | | |
| 29 6 | | | |
| 30 7 | | | |
| 31 1 | | | |

| | + | x | − | Rod |
|---|---|---|---|---|
| [illegible] +32 66 | B.C | 36 958 | | 4 6 |
| +50 | | | | 4 8 |
| T.P. | 12 152 | 48 672 | 0 438 | |
| 26 | | | | 6 4 |
| T.P. | 8 742 | 56 619 | 0 795 | |
| +50 | | | | 5 8 |
| 27. | | | | 4 6 |
| +21 | Top Bank. | | | 6 8 |
| T.P. | 2 594 | 48 903 | 10 31 | |
| T.P. | 1 004 | 38 301 | 11 666 | |
| +50 | | | | 4 5 |
| +52 } Bottom | | | | 7 8 |
| +65 } Creek. | | | | 7 8 |
| +75 Top bank. | | | | 5 1 |
| 28 | | | | 3 6 |
| 107 3 E.C. | | | | 5 3 |
| B.M. | 3 675 | 40 332 | 1 644 | |
| +50 | | | | 4 8 |
| 29 | | | | 6 7 |
| +50 | | | | 2 4 |
| T.P. | 5 144 | 43 823 | 1 653 | |
| 30 | | | | 5 4 |
| +50 | | | | 5 3 |
| 31 | | | | 2 7 |
| T.P. | 7 733 | 48 805 | 2 751 | |
| +50 | | | | 7 0 |
| 32 | | | | 6 2 |
| +50 | | | | 5 0 |

| Elev. | | |
|---|---|---|
| 32 3 | | |
| 32 1 | | |
| 36 520 | TP | |
| 42 2 | 1 | |
| 47 877 | TP | |
| 50 8 | | |
| 52 0 | | |
| 49 9 | | |
| 46 309 | TP | |
| 37 297 | T.P. | |
| 33 8 | | |
| 30 5 | | |
| 30 5 | | |
| 33 2 | | |
| 34 7 | | |
| 33 0 | | |
| 36 657 | M.B.M. on Poplar tree 25ft. Left | |
| 35 5 | M. 28+25. Elev 36 559 | |
| 33 6 | | |
| 37 9 | | |
| 38 679 | TP | |
| 38 4 | | |
| 38 5 | | |
| 41 1 | | |
| 41 072 | TP | |
| 41 8 | | |
| 42 6 | | |
| 43 8 | | |

| | + | ⊼ | − | Rod |
|---|---|---|---|---|
| +60 | | 48 805 | | 5 1/2 |
| 33 Top bank. | | | | 4 5/10 |
| +18 } Bottom | | | | 7 0 |
| +35 } Creek. | | | | 7 0 |
| +39 Top bank. | | | | 5 1/2 |
| +50 | | | | 6 0 |
| 34 | | | | 4 9/10 |
| +50 | | | | 2 4/10 |
| T.P. | 6 672 | 53 721 | 1 756 | |
| 35 | | | | 6 0 |
| +50 | | | | 6 3/10 |
| 36 | | | | 5 5/10 |
| +50 | | | | 5 8/10 |
| 37 | | | | 5 5/10 |
| +50 | | | | 4 8/10 |
| 38 | | | | 4 9/10 |
| T.P. | 6 162 | 58 805 | 1 078 | |
| +50 | | | | 7 8/10 |
| 39 | | | | 9 0 |
| +50 | | | | 7 1/2 |
| 80 75 B.C. 14° | | | | 6 7/10 |
| 40 | | | | 5 6/10 |
| +50 | | | | 5 3/10 |
| B.M. | 4 425 | 59 024 | 4 206 | |
| 41 | | | | 4 6/10 |
| T.P. | 4 639 | 62 381 | 1 282 | |
| +50 | | | | 6 1/2 |
| +83 25 E.C. | | | | 5 7/10 |

| Elev | | | |
|---|---|---|---|
| 43.7 | | | |
| 44.3 | | | |
| 41.8 | | | |
| 41.8 | | | |
| 43.7 | | | |
| 42.8 | | | |
| 43.9 | | | |
| 46.4 | | | |
| 47.049 | T.P. | | |
| 47.7 | | | |
| 47.4 | | | |
| 48.2 | | | |
| 47.9 | | | |
| 48.2 | | | |
| 48.9 | | | |
| 48.8 | | | |
| 52.643 | T.P. | | |
| 51.0 | | | |
| 49.8 | | | |
| 51.7 | | | |
| 52.1 | | | |
| 53.2 | | | |
| 53.5 | | | |
| 54.599 | | BM. on Laurel Tree | |
| 53.4 | | 5 ft. Left M 40+58 | |
| 57.742 | T.P. | | |
| 56.2 | | | |
| 56.6 | | | |

| | + | H | − | Rod |
|---|---|---|---|---|
| 42 | | 62 381 | | 5 7 |
| +50 | | | | 4 0 |
| T. P. | 3 96 | 64 74 | 1 601 | |
| 43 | | | | 5 4 |
| +50 | | | | 3 9 |
| +54 | B.C. 10 | | | 4 0 |
| 44 | | | | 5 1 |
| +50 | | | | 4 9 |
| 45 | | | | 4 4 |
| +23 | E.C. | | | 4 4 |
| +50 | | | | 3 9 |
| T. P. | 5 823 | 68 938 | 1 625 | |
| 46 | | | | 6 3 |
| +50 | | | | 6 4 |
| 47 | | | | 5 4 |
| +50 | | | | 4 6 |
| T. P. | 4 335 | 71 209 | 2064 | |
| 48 | | | | 6 8 |
| +50 | | | | 5 5 |
| 49 | | | | 5 0 |
| +50 | | | | 4 8 |
| T. P. | 5 447 | 75 241 | 1 410 | |
| 50 | | | | 8 7 |
| +50 | | | | 7 5 |
| 51 | | | | 5 3 |
| +50 | | | | 5 2 |
| 52 | | | | 5 6 |

| Elev | | | |
|---|---|---|---|
| 56 6 | | | |
| 58 3 | | | |
| 60 78 | T.P. | | |
| 59 3 | | | |
| 60 8 | | | |
| 60 7 | | | |
| 59 6 | | | |
| 59 8 | | | |
| 60 3 | | | |
| 60 3 | | | |
| 60 8 | | | |
| 63 115 | Nail in Local Tree | | |
| 62 6 | | | |
| 62 5 | | | |
| 63 5 | | | |
| 64 3 | | | |
| 66 874 | T.P. | | |
| 64 4 | | | |
| 65 7 | | | |
| 66 2 | | | |
| 66 4 | | | |
| 69 799 | T.P. | | |
| 66 5 | | | |
| 67 7 | | | |
| 69 9 | | | |
| 70 | | | |
| 69 6 | | | |

| | | | | |
|---|---|---|---|---|
| 52+50 | | 75 246 | | 4 0 |
| 53 | | | | 3 2 |
| +21 07 B.C. 4°L | | | | 2 9 |
| +50 | | | | 2 9 |
| 54 | | | | 1 7 |
| T.P. | 8 450 | 82 857 | 1039 | |
| +36 9 E.S. | | | | 9 4 |
| +50 | | | | 9 0 |
| 55 | | | | 8 5 |
| +50 | | | | 7 1 |
| 56 | | | | 6 2 |
| +50 | | | | 3 8 |
| 57 | | | | 3 0 |
| T.P. | 6010 | 87 752 | 1115 | |
| +50 | | | | 3 9 |
| 58 | | | | 5 5 |
| +50 | | | | 5 3 |
| -89 2 B.C. 1A°R. | | | | 4 7 |
| 59 | | | | 5 0 |
| +50 | | | | 3 7 |
| 60 | | | | 1 4 |
| +50 | | | | 3 1 |
| +88 5 EC | | | | 2 2 |
| 61 | | | | 2 3 |
| +50 | | | | 1 8 |
| T.P. | 6745 | 92 687 | 1810 | |
| +93 48 B.C. 10°L | | | | 5 9 |

| | | | |
|---|---|---|---|
| 71 2 | | | |
| 72 0 | | | |
| 72 3 | | | |
| 72 7 | | | |
| 73 5 | | | |
| 74 207 | T.P. | | |
| 73 5 | | | |
| 73 9 | | | |
| 76 4 | | | |
| 75 8 | | | |
| 76 7 | | | |
| 79 1 | | | |
| 79 9 | | | |
| 81 742 | T.P. | | |
| 83 9 | | | |
| 82 3 | | | |
| 82 5 | | | |
| 83 1 | | | |
| 82 8 | | | |
| 84 1 | | | |
| 86 4 | | | |
| 84 7 | | | |
| 85 6 | | | |
| 85 5 | | | |
| 85 9 | | | |
| 85 942 | | | |
| 86 8 | | | |

| | | | | |
|---|---|---|---|---|
| 62 | | 92 687 | | 6° |
| +50 | | | | 4 3 |
| 63 | | | | 4 1 |
| +50 | | | | 2 9 |
| T.P. | 3 370 | 95 167 | 0 890 | |
| 64 | | | | 4° |
| +25 31 EC | | | | 3 4 |
| +50 | | | | 3 6 |
| T.P. | 8 180 | 99 977 | 3 370 | |
| 65 | | | | 8 2 |
| +50 | | | | 2 9 |
| 66 | | | | 6 7 |
| +50 | | | | 5 5 |
| 67 | | | | 4 5 |
| +50 | | | | 4 3 |
| 68 | | | | 2° |
| +50 | | | | 1 8 |
| T.P. | 9 228 | 107 302 | 1 903 | |
| +86 31 | EC 14°L | | | 9° |
| 69 | | | | 7 9 |
| +50 | | | | 9 1 |
| +64 2 | EC | | | 8 9 |
| 70 | | | | 7 2 |
| +33 1 | B.C. 12°R | | | 6 1 |
| +50 | | | | 6 4 |
| 71 | | | | 3 1 |
| +38 7A | | | | 4 1 |

| | | | |
|---|---|---|---|
| 87 7 | | | |
| 88 4 | | | |
| 88 6 | | | |
| 89 8 | | | |
| 91 797 | T.P. | | |
| 91 2 | | | |
| 91 8 | | | |
| 91 6 | | | |
| 91 797 | T.P. | | |
| 91 8 | | | |
| 93 1 | | | |
| 93 0 | | | |
| 94 5 | | | |
| 95 5 | | | |
| 95 7 | | | |
| 98 0 | | | |
| 98 2 | | | |
| 98 074 | TP | | |
| 98 3 | | | |
| 99 4 | | | |
| 98 2 | | | |
| 98 4 | | | |
| 100 0 | | | |
| 101 2 | | | |
| 100 9 | | | |
| 104 2 | | | |
| 103 2 | Top Bank | Should be Gr. | |

| | | | | |
|---|---|---|---|---|
| 71 +42 | | 107 302 | | 8 5 |
| Water Surf. | | | | 6 0 |
| +59 74 | | | | 6 4 |
| +99 74 E.C. | | | | 7 1 |
| 72+30 | | | | 5 0 |
| T.P. | 7 405 | 112 217 | 2 490 | |
| +50 | | | | 8 1 |
| 73 | | | | 3 7 |
| +50 | | | | 1 9 |
| 74 | | | | 4 1 |
| +38 91 B.C. 14°L | | | | 4 9 |
| T.P. | 5 445 | 111 962 | 0 700 | |
| +50 | | | | 7 1 |
| 75 | | | | 6 0 |
| +50 | | | | 6 3 |
| 76 | | | | 5 1 |
| +50 | | | | 4 1 |
| B.M. | | | | 3 725 |
| 1 | | | | |
| T.P. | 6 003 | 120 675 | 2 290 | |
| 77 | | | | 5 5 |
| +40 | | | | 6 7 |
| +42 | | | | 10 0 |
| +50 | | | | 9 7 |
| +55 | | | | 9 7 |
| +60 | | | | 5 4 |
| 78 | | | | 4 8 |

| | | | |
|---|---|---|---|
| 98 8 | Bot. Cr. | | |
| 101 3 | Water Surf. | | |
| 100 9 | | | |
| 100 2 | | | |
| 102 3 | Bank | | |
| 104 812 | T.P. | | |
| 104 1 | | | |
| 108 5 | | | |
| 110 3 | | | |
| 108 1 | | | |
| 107 3 | | | |
| 111 517 | T.P. | | |
| 109 9 | | | |
| 111 0 | | | |
| 110 7 | | | |
| 111 9 | | | |
| 112 9 | | | |
| 113 237 | B.M. on R.W. Stump. 75 Lt Sta. 75+50 | | |
| 114 672 | | | |
| 115 2 | | | |
| 114 0 | | | |
| 110 7 | | | |
| 111 0 | | | |
| 111 0 | | | |
| 115 3 | | | |
| 115 9 | | | |

| | | | | |
|---|---|---|---|---|
| +50 | | 120.675 | | 39 |
| 79 | | | | 25 |
| +50 | | | | 16 |
| T.P. | 6050 | 125157 | 1568 | |
| 80 | | | | 57 |
| +4286 | | | | 52 |
| +50 | | | | 48 |
| 81 | | | | 44 |
| +50 | | | | 40 |
| 82 | | | | 30 |
| +50 | | | | 32 |
| 83 | | | | 07 |

116 8
118 2
119 1
119 107
119 5
120 0
120 4
120 8
121 2
122 2
122 0
124 5

# Grades

## Laton Lumber Co Spur

| | Elev. | Grade | cut | Fill |
|---|---|---|---|---|
| 15 | 18 1/4 | 18 9/10 | | 0 8/10 |
| +50 | 18 6/10 | 19 6/10 | | 1 0/0 |
| 16 | 19 3/10 | 20 3/10 | | 1 0/0 |
| +50 | 19 8/10 | 21 0/0 | | 1 2/10 |
| 17 | 20 9/10 | 21 7/10 | | 0 8/10 |
| +50 | 22 0/0 | 22 4/10 | | 0 4/10 |
| 18 | 23 5/10 | 23 1/10 | 0 4/10 | |
| +50 | 23 6/10 | 23 8/10 | 0 8/10 | |
| +94.06 | 25 4/10 | 24 4/10 | 1 0/0 | |
| 19 | 25 7/10 | 24 5/10 | 1 2/10 | |
| +50 | 26 9/10 | 25 2/10 | 1 7/10 | |
| 20 | 26 5/10 | 25 9/10 | 0 6/10 | |
| +50 | 26 3/10 | 26 6/10 | | 0 3/10 |
| 21 | 26 8/10 | 27 3/10 | | 0 5/10 |
| +19.2 | 25 7/10 | 27 6/10 | | 1 9/10 |
| +65.0 | 27 1/10 | 28 2/10 | | 1 1/10 |
| 22 | 27 4/10 | 28 7/10 | | 1 3/10 |
| +12.25 | 27 8/10 | 28 9/10 | | 1 1/10 |
| +50 | 27 9/10 | 29 4/10 | | 1 5/10 |
| 23 | 29 1/10 | 30 1/10 | | 1 0/0 |
| +50 | 30 0/0 | 30 8/10 | | 0 8/10 |
| 24 | 29 6/10 | 31 5/10 | | 1 9/10 |
| +50 | 30 7/10 | 32 2/10 | | 1 5/10 |
| 25 | 31 1/10 | 32 9/10 | | 1 8/10 |
| +32.56 | 32 3/10 | 33 4/10 | | 1 1/10 |
| +50 | 32 1/10 | 33 6/10 | | 1 5/10 |
| 26 | 42 2/10 | 34 3/10 | 7 9/10 | |
| +50 | 50 8/10 | 35 0/0 | 15 8/10 | |

+1.40

| | Elev | Grade | Cut | Fill |
|---|---|---|---|---|
| 27 | 52.0 | 35.7 | 16.3 | |
| +21.00 | 49.8 | 36.0 | 13.8 | |
| +50 | 33.8 | 36.4 | | 2.6 |
| +75.00 | 33.5 | 36.7 | | 3.5 |
| 28 | 34.7 | 37.1 | | 2.4 |
| +07.3 | 33.0 | 37.2 | | 4.2 |
| +50 | 35.5 | 37.8 | | 2.3 |
| 29 | 33.6 | 38.5 | | 4.9 |
| +50 | 37.9 | 39.2 | | 1.3 |
| 30 | 38.4 | 39.7 | | 1.5 |
| +50 | 38.5 | 40.6 | | 2.1 |
| 31 | 41.1 | 41.3 | | 0.2 |
| +50 | 41.8 | 42.0 | | 0.2 |
| 32 | 42.6 | 42.1 | | 0.1 |
| +50 | 43.8 | 43.4 | 0.4 | |
| +60 | 43.7 | 43.1 | 0.6 | |
| 33 | 44.3 | 44.1 | 0.2 | |
| +39 | 43.7 | 44.6 | | 0.9 |
| +50 | 42.8 | 44.8 | | 2.0 |
| 34 | 43.9 | 45.5 | | 1.6 |
| +50 | 46.4 | 46.2 | 0.2 | |
| 35 | 47.1 | 46.9 | 0.8 | |
| +50 | 47.4 | 47.6 | | 0.2 |
| 36 | 48.2 | 48.3 | | 0.1 |
| +50 | 47.9 | 49.0 | | 1.1 |
| 37 | 48.2 | 49.7 | | 1.5 |
| +50 | 48.9 | 50.4 | | 1.5 |
| 38 | 48.8 | 51.1 | | 2.3 |

| | Elev | Grade | Cut | Fill |
|---|---|---|---|---|
| 38+50 | 51.0 | 51.8 | | 0.8 |
| 39 | 49.8 | 52.5 | | 2.7 |
| +50 | 51.7 | 53.2 | | 1.5 |
| +80 25 B.C. | 52.1 | 53.6 | | 1.5 |
| 40 | 53.2 | 53.9 | | 0.7 |
| +50 | 53.5 | 54.6 | | 1.1 |
| 41 | 53.4 | 55.3 | | 1.9 |
| +50 | 56.0 | 56.0 | | Grade |
| +83 25 E.C. | 56.6 | 56.5 | | Grade |
| 42 | 56.6 | 56.7 | | 0.1 |
| +50 | 58.3 | 57.4 | 0.9 | |
| 43 | 59.3 | 58.1 | 1.2 | |
| +50 | 60.8 | 58.8 | 2.0 | |
| +54 47 B.C. | 60.7 | 58.9 | 1.8 | |
| 44 | 59.5 | 59.5 | | Grade |
| +50 | 59.8 | 60.2 | | 0.4 |
| 45 | 60.3 | 60.9 | | 0.6 |
| +23 9 E.C. | 60.3 | 61.2 | | 0.9 |
| +50 | 60.8 | 61.6 | | 0.8 |
| 46 | 62.1 | 62.3 | 0.3 | |
| +50 | 62.5 | 63.0 | | 0.5 |
| 47 | 63.5 | 63.7 | | 0.2 |
| +50 | 64.4 | 64.4 | | Grade |
| 48 | 64.4 | 65.1 | | 0.7 |
| +50 | 65.7 | 65.8 | | 0.1 |
| 49 | 66.2 | 66.5 | | 0.7 |
| +50 | 66.4 | 67.2 | | 0.8 |
| 50 | 66.5 | 67.9 | | 1.4 |

+140

| | Elev. | Grade | Cut | Fill |
|---|---|---|---|---|
| 50+50 | 67.7 | 68.6 | | 0.9 |
| 51 | 69.9 | 69.3 | 0.6 | |
| +50 | 70.0 | 70.0 | Grade | |
| 52 | 69.6 | 70.7 | | 1.1 |
| +50 | 71.2 | 71.4 | | 0.2 |
| 53 | 72.1 | 72.1 | Grade | |
| +21.07 B.C. | 72.4 | 72.4 | Grade | |
| +50 | 72.3 | 72.8 | | 0.5 |
| 54 | 73.5 | 73.5 | Grade | |
| +36.9 E.S. | 73.5 | 74.0 | | 0.5 |
| +50 | 73.9 | 74.2 | | 0.3 |
| 55 | 76.4 | 74.2 | 1.5 | |
| +50 | 75.8 | 75.6 | Grade | |
| 56 | 76.7 | 76.3 | 0.4 | |
| +50 | 79.1 | 77.2 | 1.9 | |
| 57 | 79.9 | 78.1 | 1.8 | |
| +50 | 80.9 | 78.9 | 5.0 | |
| 58 | 82.3 | 79.8 | 2.5 | |
| +50 | 82.5 | 80.7 | 1.8 | |
| +89.7 B.C. | 83.1 | 81.4 | 1.7 | |
| 59 | 82.8 | 81.6 | 1.2 | |
| +50 | 84.1 | 82.4 | 1.7 | |
| 60 | 86.4 | 83.3 | 3.1 | |
| +50 | 84.7 | 84.2 | 0.5 | |
| +88.5 E.C. | 85.1 | 84.9 | 0.7 | |
| 61 | 85.5 | 85.1 | 0.4 | |
| +50 | 85.9 | 85.9 | Grade | |

| | Elev | Grade | Cut | Fill |
|---|---|---|---|---|
| 61+93 18 B.C. | 869 | 867 | Grade | |
| 62 | 817 | 868 | Grade | |
| +50 | 884 | 876 | 08 | |
| 63 | 886 | 886 | Grade | |
| +50 | 898 | 894 | 04 | |
| 64 | 912 | 903 | 09 | |
| +25 31 E.C. | 918 | 907 | 11 | |
| +50 | 916 | 913 | 03 | |
| 65 | 918 | 921 | | 03 |
| +50 | 929 | 929 | Grade | |
| 66 | 933 | 938 | | 05 |
| +50 | 945 | 947 | | 02 |
| 67 | 956 | 956 | Grade | |
| +50 | 957 | 964 | | 07 |
| 68 | 980 | 973 | 07 | |
| +50 | 982 | 982 | Grade | |
| +81 81 B.C. | 983 | 988 | | 05 |
| 69 | 994 | 991 | 03 | |
| +50 | 982 | 999 | | 17 |
| +64 2 E.C. | 984 | 1002 | | 18 |
| 70 | 1000 | 1008 | | 08 |
| +33 1 B.C. | 1012 | 1014 | | 02 |
| +50 | 1009 | 1016 | | 07 |
| 71 | 1042 | 1026 | 16 | |
| +38 74 | 1033 | 1033 | Grade | |
| +39 74 | 1009 | 1036 | | 27 |
| 72 | 1002 | 1043 | | 41 |

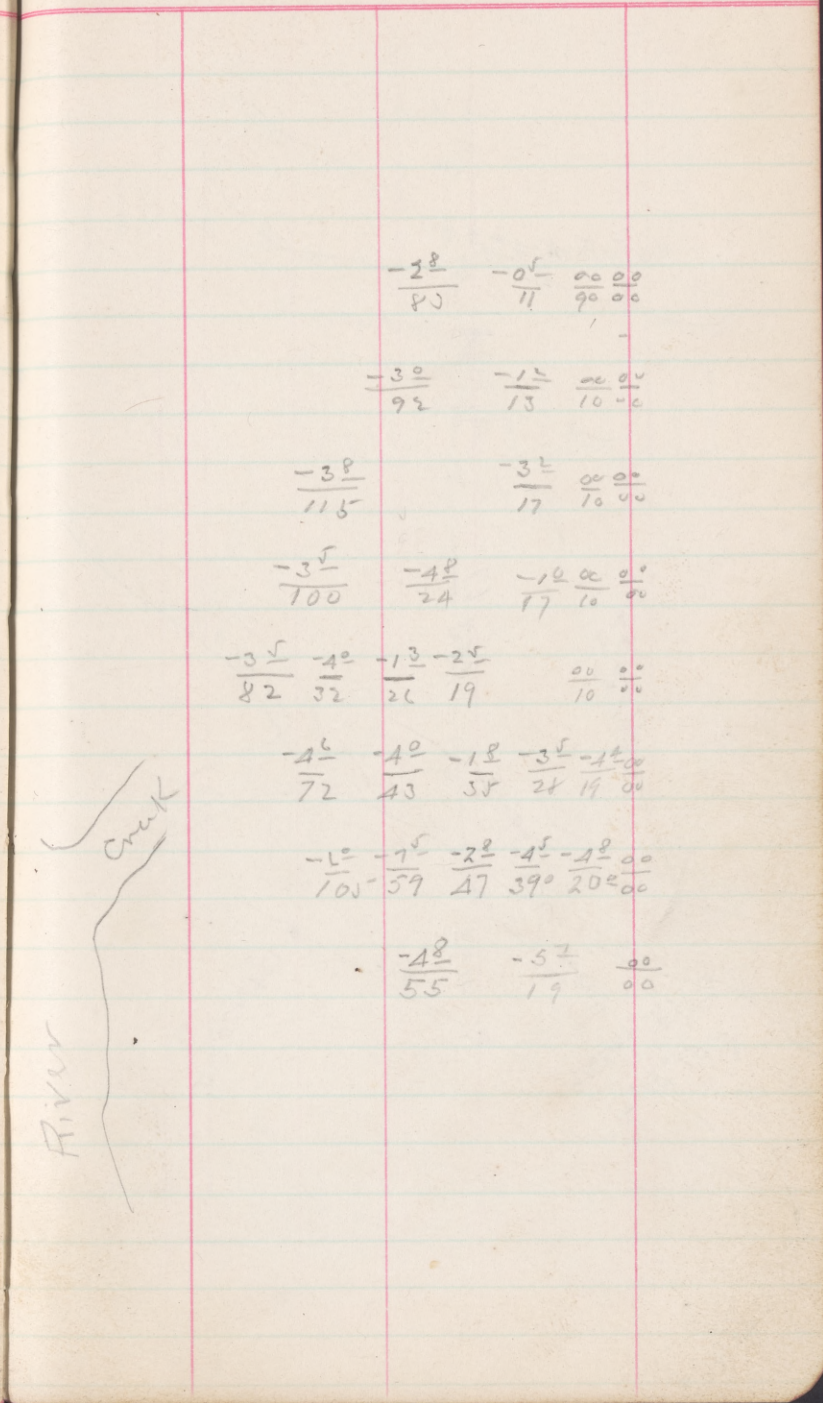
+175

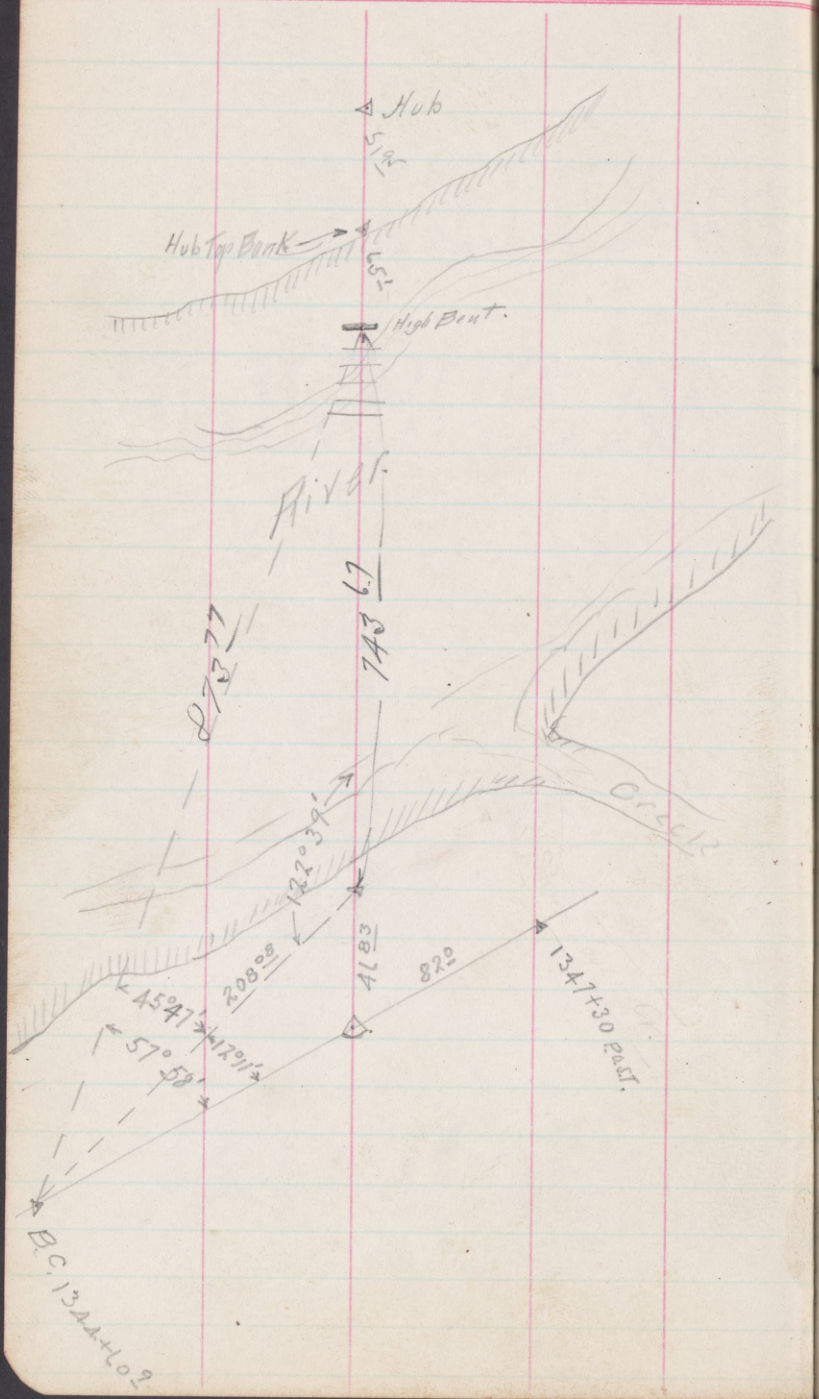
| | Elev | Grade | Cut | Fill |
|---|---|---|---|---|
| 72+30 | 102 3 | 104 8 | | 2 5 |
| +50 | 104 1 | 105 3 | | 1 2 |
| 73 | 108 5 | 106 1 | 2 4 | |
| +50 | 110 3 | 106 9 | 3 4 | |
| 74 | 108 1 | 107 8 | 0 3 | |
| +38 96 | 107 3 | 108 5 | | 1 2 |
| 74+50 | 109 9 | 108 7 | 1 2 | |
| 75 | 111 0 | 109 6 | 1 4 | |
| +50 | 110 7 | 110 4 | 0 3 | |
| 76 | 111 9 | 111 3 | 0 6 | |
| +50 | 112 9 | 112 0 | 0 6 | |
| 77 | 115 2 | 113 1 | 2 1 | |
| +40 | 114 0 | 113 8 | 0 2 | |
| +50 | 111 0 +1 75 | 113 9 | | 2 9 |
| 78 | 115 9 | 114 8 | 1 1 | |
| +50 | 116 8 | 115 7 | 1 1 | |
| 79 | 118 2 | 116 6 | 1 6 | |
| +50 | 119 1 | 117 4 | 1 7 | |
| 80 | 119 5 | 118 3 | 1 2 | |
| +42 86 E.C | 120 0 | 119 0 | 1 0 | |
| +50 | 120 4 | 119 2 | 1 2 | |
| 81 | 120 8 | 120 1 | 0 7 | |
| +50 | 121 2 | 120 9 | 0 3 | |
| 82 | 122 2 | 121 8 | 0 4 | |
| +50 | 122 | 122 68 | 0 | 0 7 |
| 83 | 124 5 | 123 55 | 1 0 | 0 |

# Spur for P. P. & K.

M

| | | | | |
|---|---|---|---|---|
| 1351 | | | Bank | 51 |
| +85.4 | C.C. | | Bank | 54 |
| +50 | | | Bank. | 65.0 |
| +30 | Big Tree. 28.0 6 ft Tree | | | |
| 1350 | Grade 10 | | Bank | 83° |
| +50 | Grade. 10° | | Bank | 92° |
| 1349 | Grade 10° | | Bank | 115 |
| +50 | Grade 10° | | Bank. | 100 |
| 1348 | Grade 10.0 | | Bank | 82.0 |
| +50 | Grade. 10.0 | | 72.0 B. Creek | |
| | Mouth of S.N. Creek | | | |
| 1347 | Grade 8 | | Bank | 105 |
| +40.9 C.C. | Top Grade 9° | | Bank | 55 |
| | Trees at 9° at | | | |
| 1346+10.9 | | 13° | | 46° |
| +80.9 | Top Grade 12° | | Bank | 39 |
| +50.9 | Top Grade 11° | | Bank | 35 |
| 1345+20.9 | Top G. 12° | | Old. Bank | 24 |
| +90.9 | " 12° Lt | | | |
| 1344+60.9 B.C. | Bank 8.5 Lt. | | | |


Creek
River


Hub
Hub Top Bank
High Bent.
River
Creek
122°39'
208°08
82°
1347+30 Past.
45°47'
12°11'
57°58'
B.C. 1344+60

# Re Alignment of Laton Spur.

Aug 11 - 1913

(5)

| | | | |
|---|---|---|---|
| 1+98.83 E.C | 9°56½ | ✓ | △19°53' |
| 1+50 | 7°30 | ✓ | St 71.78 |
| 1 | 5°00 | ✓ | St 100.46 |
| +50 | 2°30 | ✓ | |
| 0+00 B.C. 1° Rt. | 0°00 | ✓ | |

(6)

| | | |
|---|---|---|
| 1+02.5 E.C. | 2°03' | |
| 1+00 | 2°00 | △4°06' |
| +50 | 1°00 | St 51.27 |
| 0+00 B.C. 4° Lt. | 0°00 | |

(7)

| | | | |
|---|---|---|---|
| 1+89.3 E.C. | 13°15 | ✓ | |
| +50 | 10°30 | ✓ | △26°30 |
| 1 | 7°00 | ✓ | St 96.43 |
| +50 | 3°30 | ✓ | |
| 0+00 B.C. 14° Rt. | 0°00 | ✓ | |

+02.5
4 | 4.10°0
8

| | | | |
|---|---|---|---|
| 0+98 19 | E.C. 6° 54½ | | |
| 0+75 | 5° 15' | Δ 13° 49' | |
| 0+50 | 3° 30 | St. 49 62 | (9) |
| 0+25 | 1° 45 | | |
| 0+00 | B.C. 14° | | |
| | | | |
| 2+17 03 | E.C. 10° 52 | | |
| 2+00 | 10° 00' | | |
| 1+50 | 7° 30' | Δ 21° 44' | |
| 1 | 5° 00' | St 110 02 | (8) |
| 0+50 | 2° 30' | | |
| 0+00 | B.C. 10° 14 | | |
| | | | |
| 1+03 33 | E.C. 14° 14' | | |
| 2 | 14° 00' | | |
| 1+50 | 10° 30 | | |
| 1 | 7° 00 | Δ 28° 28' | |
| 0+50 | 3° 30 | St 103 88 | (4) |
| 0+00 | B.C. 14° 14 | | |
| | | | |
| 0+84 16 | E.C. 1° 41' | | |
| 0+50 | 1° 00 | Δ 3° 22 | 5½ |
| 0+00 | B.C. 4° 14 | St 42 1 | |

1+67.1 E.C. 11°42'

1+50 10°30'

1+00 7°00'

0+50 3°30'

0+00 B.C. 14° R.

Δ 25°24'

St & A 80

$$
\begin{array}{r}
23.24 \\
\hline
17 \overline{)\,23.4} \\
14 \\
\hline
94 \\
84 \\
\hline
100 \\
98 \\
\hline
2
\end{array}
$$

Line Change Markham Br.

near rocky Point.

July - 1913

| | | | | |
|---|---|---|---|---|
| 1227+00 | R.O.T. | Revaluation Change | | |
| 1236+11$^{2}$ | B.C. 9° Rt. | | | |
| | | △ 14°23' | | |
| 1237+71$^{0}$ | E.C. | St. = 80$^{34}$ | | |
| 1239+18$^{98}$ | B.C. 15 Lt. | | | |
| | | △ 29°49' | | |
| | | St. 101$^{76}$ | | |
| 1241+17$^{68}$ | E.C. | | | |
| 1242+13$^{44}$ | B.C. 15 Rt. | | | |
| | | △ 38°11' | | |
| | | St. 132$^{3}$ | | |
| 1244+67$^{99}$ | E.C. | | | |
| 1245+19$^{43}$ | B.C. | 4°30' Lt | | |
| | | △ 13°17½' | | |
| | | St. 148$^{45}$ | | |
| 1248+14$^{93}$ | E.C. | | | |
| 1248+15$^{1}$ | R.O.T. | | | |

(6V)

347
15.1
496
24.9

1321+15.2 BC
5+24.9
1317+90.9 End 60# Steel.

0J 13
14 50
0.1J

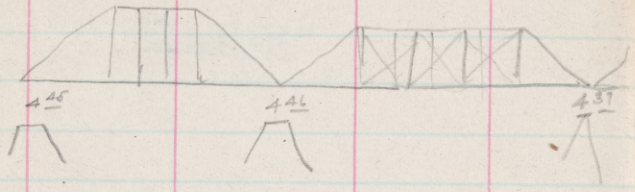
1355+44 55
8 729 to Pt Stub Sw
1346+71 65

Pitcher

Scraton 989 60 fs of 56# Sw
9 fs #9 frog.
P.S.C. 812 60 fs 56 Sw

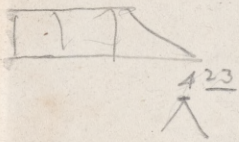
Doda. Spur.

Scraton 989 120 ft 56# Sw




Duncan Mills Bridge

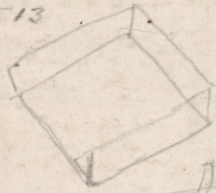
76-E


1
23

9.8
3.8
6.0

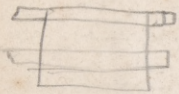
7
1.55
5.45
2.6
6.1
3.2
9.3

487
513



59
2.1
2.8
4.8
7.6

40
15
20
75



1340 + 50
1323

1750
600

7.50
.14

1352
1346
6

2350

N.G. Cars (#5322, 5535, 5513) Markham Branch

N.G. Cars {#5380, 5509, 5346} Willo Creek Branch

-05
11
62
1881
1913

Mike Burnglir

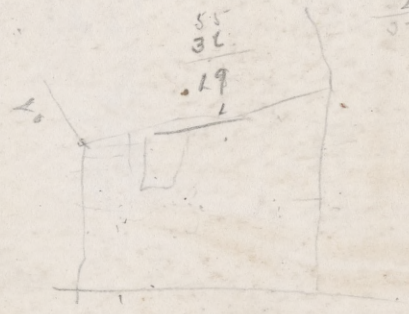
Pedro López

22
15
7
17
247

27
7
32

11
22
33

55
33
22
4
18

22
14
36
4
32

55
36
19
1